

50376  
1980  
184-2

N° d'ordre : 253

50376  
1980  
184-2

# THÈSE

présentée à

L'UNIVERSITE DES SCIENCES ET TECHNIQUES DE LILLE

pour obtenir le titre de

DOCTEUR INGÉNIEUR

EN MECANIQUE

PAR

Alain LEBLANC

CALCUL DE FACTEURS D'INTENSITE DE CONTRAINTES

DANS UN DISQUE ET UN ANNEAU CHARGES DIAMÉTRALEMENT

AVEC FISSURES SYMÉTRIQUES DANS LE PLAN DE CHARGEMENT

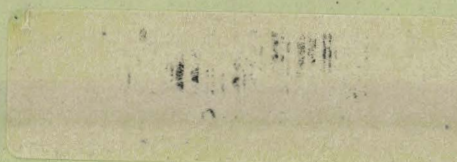
ANNEXES



Soutenu le 14 Novembre 1980.

## JURY

MM. ESCAIG	UST Lille	Président
HENRY	UST Lille	Rapporteur
CORNET	I.P.G.	Examineur
PARSY	UST Lille	Examineur
DUFFAUT	B.R.G.M.	Examineur



ANNEXE A1

DISQUE COMPORTANT UNE FISSURE CENTRALE

MÉTHODE DE SUPERPOSITION



```

DIMENSION TET(11),TET1(11),TET2(11),B(11),Y(11),X(11),H(11),Q(11)
DIMENSION RX(10),RY(10)
DIMENSION R(20),A(20,20),R01(11),R02(11)
DIMENSION TS(21),COF(21,11)
INTEGER P
REAL K1,CB(21,21),KO ,LW
DATA LC/7/,IMP/8/
DATA TET(1)/0./,TET1(1)/0./,TET2(1)/0./,B(1)/0./,Y(1)/0./,X(1)/1./,
DATA Q(1)/0./
1 READ(LC,10)AF,M
10 FORMAT(F3.1,I2)
WRITE(IMP,15)AF
15 FORMAT(1H0,55X,'A=',F3.1,3(/))
PI=4*ATAN(1.)
C=-1/(2*PI)

```

C  
C  
C  
C

CALCUL DES PARAMETRES  
\*\*\*\*\*

```

H(1)=1-AF*AF
R01(1)=1-AF
R02(1)=1+AF
M1=M+1
M2=2*M
WRITE(IMP,16)
16 FORMAT(3X,'N',6X,'TET(N)',5X,'TET1(N)',5X,'TET2(N)',6X,'B(N)',8X,'
1Y(N)',8X,'X(N)',7X,'R01(N)',6X,'R02(N)',7X,'H(N)',8X,'Q(N)')
DO 100 N=2,M1
TET(N)=(N-1)*PI/M2
SI=SIN(TET(N))
9 CO=COS(TET(N))
IF(TET(N).EQ.1.570796)CO=0.00
TET1(N)=ATAN(SI/(CO-AF))
IF(TET1(N)2,5,3
2 TET1(N)=PI+TET1(N)
3 TET2(N)=ATAN(SI/(CO+AF))
B(N)=(TET1(N)+TET2(N))/2.
Y(N)=SI
X(N)=CO
R01(N)=SQRT(Y(N)*Y(N)+(X(N)-AF)*(X(N)-AF))
R02(N)=SQRT(Y(N)*Y(N)+(X(N)+AF)*(X(N)+AF))
H(N)=SQRT((1+AF*AF)*(1+AF*AF)-(4*AF*AF*CO*CO))
Q(N)=SI/SQRT(H(N))
WRITE(IMP,17)N,TET(N),TET1(N),TET2(N),B(N),Y(N),X(N),R01(N),R02(N)
1,H(N),Q(N)
17 FORMAT(3X,I2,10(3X,F9.7))
100 CONTINUE

```

C  
C  
C  
C

CALCUL DES COMPOSANTES DES RESULTANTES DE ETAT B SUR CHAQUE SEGMENT  
\*\*\*\*\*

```

DO 200 I=1,M
RX(I)=2*CO*(Y(I+1)-Y(I)+Q(I)*COS(TET(I)-B(I))-Q(I+1)*COS(TET(I+1)-B
1(I+1)))

```

```

RY(I)=2*C*(X(I)-X(I+1))+SQRT(H(I+1))*COS(B(I+1))-SQRT(H(I))*COS(B
1(I))+Q(I+1)*SIN(TET(I+1))-B(I+1))-Q(I)*SIN(TET(I))-B(I))
200 CONTINUE
WRITE(IMP,90)
90 FORMAT(1H0,10X,'COMPOSANTES HORIZONTALES DES RESULTANTES DE L''ETA
1T B',///)
WRITE(IMP,110)((I,RX(I)),I=1,M)
110 FORMAT(1H0,50X,'RX(',I2,')=',E13.7)
WRITE(IMP,25)
WRITE(IMP,120)
120 FORMAT(1H0,10X,'COMPOSANTES VERTICALES DES RESULTANTES DE L''ETAT
1E',///)
WRITE(IMP,130)((I,RY(I)),I=1,M)
130 FORMAT(1H0,50X,'RY(',I2,')=',E13.7)
C
C
C
C
CALCUL DES COEFFICIENTS DE LA MATRICE (SAUF GAMMA(I,J))
*****
DO 300 I=1,M
DO 300 J=1,M
K=2*I-1
L=2*I-2
A(J,I)=2*(Q(J+1)*COS(K*TET(J+1))-B(J+1))-Q(J)*COS(K*TET(J))-B(J))
A(J,I+M)=2*((SIN(K*TET(J+1))-SIN(K*TET(J)))/K+Y(J+1))*COS(L*TET(J+1)
1)-Y(J)*COS(L*TET(J))
A(J+M,I+M)=2*(Y(J)*SIN(L*TET(J))-Y(J+1)*SIN(L*TET(J+1)))
300 CONTINUE
C
C
C
C
CALCUL DES COEFFICIENTS GAMMA(I,J)
*****
CALL COMBI(CB,20)
DO 700 N=1,M
IF(N.E.1)GO TO 4
DO 1000 J=1,M
A(J+M,1)=2*(SQRT(H(J))*COS(B(J))-SQRT(H(J+1))*COS(B(J+1))+Q(J)*
1SIN(TET(J))-B(J))-Q(J+1)*SIN(TET(J+1))-B(J+1))
1000 CONTINUE
4 N1=N-1
DO 800 F=0,N1
EX=2*F+1
LW=1
IF(F.NE.0)LW=CB(N1,F)
KD=LW*AF**(2*(N1-F))
IF(F.EG.N1)GO TO 6
DO 800 J=1,M
COF(1,J)=0.
COF(F+2,J)=COF(F+1,J)+((2*KD)/EX)*(H(J)**(EX/2))*COS(EX*B(J))-H(J+1)**(
1)**(EX/2))*COS(EX*B(J+1))
800 CONTINUE
6 DO 900 J=1,M
A(J+M,N)=COF(N,J)+2*((KD*H(J)**(EX/2))*COS(EX*B(J)))/EX-(KD*H(J+1)

```

```

1** (EX/2)*COS(EX*B(J+1))/EX)+2*((Q(J)*SIN(EX*TET(J)-B(J)))-(Q(J+1)
1*SIN(EX*TET(J+1)-B(J+1)))

```

```

900 CONTINUE
700 CONTINUE

```

C  
C  
C  
C

```

RESOLUTION DU SYSTEME
*****

```

```

WRITE(IMP,140)
140 FORMAT(1H0,10X,'MATRICE DES COEFFICIENTS',///)
WRITE(IMP,80)((A(I,J),J=1,M2),I=1,M2)
80 FORMAT(10(E11.4,1X))
WRITE(IMP,25)
DO 210 I=1,M
R(I)=-RX(I)
R(I+M)=-RY(I)

```

```

210 CONTINUE

```

```

M=M2
N=1
EPS=0.0000001
CALL GELG(R,A,M,N,EPS,IER)
IF(IER.NE.0)GO TO 55
WRITE(IMP,20)

```

```

20 FORMAT(1H0,35X,'COEFFICIENTS DES TERMES DE LA PREMIERE SERIE',///)
M=M2/2

```

```

WRITE(IMP,30)(I,R(I),I=1,M)
30 FORMAT(1H0,50X,'A(',I2,')=',F10.6,/)
WRITE(IMP,25)

```

```

25 FORMAT(1H0,///)
WRITE(IMP,40)

```

```

40 FORMAT(1H0,35X,'COEFFICIENTS DES TERMES DE LA DEUXIEME SERIE',///)
WRITE(IMP,50)(J,R(J+M),J=1,M)

```

```

50 FORMAT(1H0,50X,'B(',I2,')=',F10.6,/)

```

C  
C  
C  
C

```

CALCUL DU COEFFICIENT D'INTENSITE DE CONTRAINTES
*****

```

```

TS(1)=0.
DO 600 I=2,M1
J=I-1
TS(I)=TS(J)+(R(J)*AF**(2*J-1))/AF

```

```

600 CONTINUE

```

```

K1=1.+TS(J+1)*2*PI
WRITE(IMP,45)
45 FORMAT(1H0,35X,'COEFFICIENT D'INTENSITE DE CONTRAINTES')
WRITE(IMP,65)K1

```

```

65 FORMAT(1H0,50X,'K1=',F7.5,)
55 WRITE(IMP,60)IER
60 FORMAT(1H0,10X,'IER=',I3)
5 WRITE(IMP,35)

```

```

35 FORMAT(1H0'ERREUR SUR TETA1')
70 STOP
END

```

```
SUBROUTINE COMBI(CB,M)
REAL DI(21),NU(21),CB(21,21)
CB(1,1)=1
DO 301 J=2,M
NU(1)=J
CB(J,1)=J
DO 101 I=2,M
IF(I.GT.J)GO TO 201
DI(1)=1
DI(I)=DI(I-1)*I
NU(I)=NU(I-1)*(J-I+1)
CB(J,I)=NU(I)/DI(I)
101 CONTINUE
201 CB(J,I)=1
301 CONTINUE
RETURN
END
```

R(S)

## ANNEXE A2

DISQUE COMPORTANT DEUX FISSURES SYMÉTRIQUES

MÉTHODE DE SUPERPOSITION

## SUBROUTINE INT

```

COMMON TETA(101),RPRO(101),STET(101),A(11,101),AP(11,11),CF(11,11)
COMMON CX(11),CY(11),TSB1(12),TSB2(12),Y(11),Z(11),ANUM(11,10)
COMMON RX(10),RY(10),R(21)
COMMON B(21,21),X(11),SUP(11)
COMMON FI,MM,M1,LC,IMP,NM,B22,B12,CON,CONS,B1,B2,M,GAMMA

```

```

C
C  CALCUL NUMERIQUE DES INTEGRALES

```

```

C *****

```

```

H=PI/(20*M)

```

```

NDIM=11

```

```

L=0

```

```

NM=10*M-9

```

```

DO 300 I=1,NM,10

```

```

L=L+1

```

```

DO 302 N=1,M1

```

```

DO 301 J=1,11

```

```

301 Y(J)=A(N,I+J-1)

```

```

CALL QSF(H,Y,Z,NDIM)

```

```

302 ANUM(N,L)=Z(11)

```

```

300 CONTINUE

```

```

UPS1=B1*1.E-03

```

```

UPS2=B2*1.E-03

```

```

X(1)=B1+UPS1

```

```

H=(B2-B1-UPS1-UPS2)/10

```

```

V=SQRT(B22-B12)

```

```

DO 105 N=1,M1

```

```

DO 106 I=1,11

```

```

IF(I.GT.1)X(I)=X(I-1)+H

```

```

X2=X(I)*X(I)

```

```

PD=SQRT((X2-B12)*(B22-X2))

```

```

106 Y(I)=X(I)**(2*N-1)/PD

```

```

CALL QSF(H,Y,Z,NDIM)

```

```

S1=SQRT(2*UPS1)*(B1**(2*N-1))/(V*SQRT(B1))

```

```

S2=SQRT(2*UPS2)*(B2**(2*N-1))/(V*SQRT(B2))

```

```

SUP(N)=Z(11)+S1+S2

```

```

105 CONTINUE

```

```

RETURN

```

```

END

```

R(S)



## SUBROUTINE GAM

COMMON TETA(101),RPRO(101),STET(101),A(11,101),AP(11,11),CP(11,11)

COMMON CX(11),CY(11),TSB1(12),TSB2(12),Y(11),Z(11),ANUM(11,10)

COMMON RX(10),RY(10),R(21)

COMMON B(21,21),X(11),SUP(11)

COMMON PI,MM,M1,LC,IMP,NM,B22,B12,CON,CONS,B1,B2,M,GAMMA

## CALCUL DE GAMMA

\*\*\*\*\*

AK=SQRT(B22-B12)/B2

CALL CEL1(RES,AK,IER)

F=RES

AZ=1.

BZ=1.-AK\*AK

CALL CEL2(RES,AK,AZ,BZ,IER)

E=RES

GAMMA=B22\*E/F-(B12+B22)/2.

WRITE(IMP,50)

50 FORMAT(////)

## CALCUL DES RESULTANTES DE L'ETAT B

\*\*\*\*\*

CON=(B12+B22)/2.+GAMMA

WRITE(IMP,70)

70 FORMAT(1H,30X,'ARC',20X,'RX',20X,'RY',/)

CONS=-1./PI

DO 400 I=1,M

RX(I)=CONS\*(CY(I+1)\*(1.-AP(2,I+1)+CON\*AP(1,I+1))-CY(I)\*(1.-AP(2,I

S)+CON\*AP(1,I)))

RY(I)=CONS\*(CX(I)-CX(I+1)+ANUM(2,I)-CON\*ANUM(1,I))+CY(I+1)\*CONS\*(

SCP(2,I+1)-CON\*CP(1,I+1))-CY(I)\*CONS\*(CP(2,I)-CON\*CP(1,I))

WRITE(IMP,80)I,RX(I),RY(I)

80 FORMAT(1H0,31X,I2,17X,F9.6,13X,F9.6,//)

400 CONTINUE

RETURN

END

S)

## SUBROUTINE RESOL

```

COMMON TETA(101),RPRO(101),STET(101),A(11,101),AP(11,11),CP(11,11)
COMMON CX(11),CY(11),TSB1(12),TSB2(12),Y(11),Z(11),ANUM(11,10)
COMMON RX(10),RY(10),R(21)
COMMON B(21,21),X(11),SUP(11)
COMMON PI,MM,M1,LC,IMP,NM,R22,R12,CON,CONS,R1,R2,M,GAMMA
M3=2*M+1

```

```

C
C  CALCUL DES COEFFICIENTS ET DEFINITION DE LA MATRICE DU SYSTEME
C  *****
DO 500 I=1,M1
DO 501 J=1,M
B(J,I)=2*(CY(J+1)*AP(I,J+1)-CY(J)*AP(I,J))
501 B(J+M1,I)=-2*ANUM(I,J)+2*(CY(J)*CP(I,J)-CY(J+1)*CP(I,J+1))
500 B(M1,I)=SUP(I)
DO 502 I=1,M
DO 503 J=1,M
K=2*I-1
L=2*I-2
IS=10*J+1
II=10*(J-1)+1
B(J,I+M1)=2*(SIN(K*TETA(IS))-SIN(K*TETA(II)))/K+2*(CY(1+1)*COS(L*
STETA(IS))-CY(J)*COS(L*TETA(II)))
503 B(J+M1,I+M1)=2*(CY(J)*SIN(L*TETA(II))-CY(J+1)*SIN(L*TETA(IS)))
502 B(M1,I+M1)=0.
WRITE(IMP,110)
110 FORMAT(///)

```

```

C
C  RESOLUTION DU SYSTEME
C  *****
DO 600 I=1,M
R(I)=-RX(I)
R(M1+I)=-RY(I)
600 CONTINUE
R(M1)=0.
L=M3
N=1
EPS=0.0000001
CALL GELB(R,B,L,N,EPS,IER)
IF(IER.NE.0)GO TO 15
RETURN
15 WRITE(IMP,160)IER
160 FORMAT(1X,'ERREUR DANS LA RESOLUTION DU SYSTEME : IER=',13)
STOP
END

```

(S)

```

COMMON TETA(101),RPRO(101),SLEI(101),A(11,101),AP(11,11),CP(11,11)
COMMON CX(11),CY(11),TSB1(12),TSB2(12),Y(11),Z(11),ANUM(11,10)
COMMON RX(10),RY(10),R(21)
COMMON B(21,21),X(11),SUP(11)
COMMON PI,MM,M1,LC,IMP,NM,B22,B12,CON,CONS,B1,B2,M,GAMMA
DATA TETA(1),SLEI(1),LC,IMP/0.,0.,7,8/
DATA A(1,1),A(2,1),A(3,1),A(4,1),A(5,1),A(6,1)/0.,0.,0.,0.,0.,0./
DATA A(7,1),A(8,1),A(9,1),A(10,1),A(11,1)/0.,0.,0.,0.,0./
DATA CP(1,1),CP(2,1),CP(3,1),CP(4,1),CP(5,1)/0.,0.,0.,0.,0./
DATA CP(6,1),CP(7,1),CP(8,1),CP(9,1),CP(10,1)/0.,0.,0.,0.,0./
DATA CP(11,1)/0./
DATA CX(1),CY(1)/1.,0./
READ(LC,10)B2,B1,M
10 FORMAT(2(F4.2),12)
WRITE(IMP,20)B2,B1,M
20 FORMAT(1H,30X,'B2=',F4.2,10X,'B1=',F4.2,10X,'M=',12,///)

```

C

C CALCUL DES PARAMETRES AUX BORNES DES ARCS D'INTEGRATION

C \*\*\*\*\*

```

B22=B2*B2
B12=B1*B1
PI=4*ATAN(1.)
M1=M+1
MM=10*M+1
DO 100 I=1,MM
IF(I.NE.1)GO TO 1
R01=1.+B2
R02=1.+B1
R03=1.-B1
R04=1.-B2
RPRO(I)=SQRT(R01*R02*R03*R04)
GO TO 100

```

```

1 TETA(I)=TETA(I-1)+PI/(20*M)
SI=SIN(TETA(I))
CO=COS(TETA(I))
TETA1=ATAN(SI/(CO+B2))
TETA2=ATAN(SI/(CO+B1))
TETA3=ATAN(SI/(CO-B1))
IF(TETA3)2,3,4
2 TETA3=PI+TETA3
4 TETA4=ATAN(SI/(CO-B2))
IF(TETA4)5,3,6
5 TETA4=PI+TETA4
6 SLEI(I)=(TETA1+TETA2+TETA3+TETA4)/2.
R01=SI/SIN(TETA1)
R02=SI/SIN(TETA2)
R03=SI/SIN(TETA3)
R04=SI/SIN(TETA4)
RPRO(I)=SQRT(R01*R02*R03*R04)
DO 101 J=1,M1
101 A(J,1)=-SIN((2*J-1)*TETA(I)-SLEI(I))/RPRO(I)
100 CONTINUE

```

C

C CALCUL DES PARAMETRES AUX BORNES DES ARCS DE DIVISION

```

C *****
AP(1,1)=1./RPRO(1)
DO 102 I=2,M1
102 AP(I,1)=AP(1,1)
J=1
DO 200 I=11,MM,10
J=J+1
CX(J)=COS(TE1A(I))
CY(J)=SIN(TE1A(I))
DO 201 N=1,M1
AP(N,J)=COS((2*N-2)*TE1A(I)-STET(1))/RPRO(1)
201 CP(N,J)=SIN((2*N-2)*TE1A(I)-STET(1))/RPRO(1)
200 CONTINUE
CALL LINK('B4')
CALL LINK('B5')
CALL LINK('B6')

C
C CALCUL DES COEFFICIENTS D'INTENSITE DE CONTRAINTE
C *****
TSB1(1)=0.
TSB2(1)=0.
DO 700 I=1,M1
TSB1(I+1)=TSB1(I)+R(I)*H1** (2*I-3)
TSB2(I+1)=TSB2(I)+R(I)*H2** (2*I-3)
700 CONTINUE
WRITE (IMP,180)
180 FORMAT (///,36X,'COEFFICIENTS D'INTENSITE DE CONTRAINTE',//)
PIB1=SQRT(P1*B1)
PIB2=SQRT(P1*B2)
DEN1=SQRT(B22-B12)
VRK1B1=-(((B12-B22)/2.-GAMMA)/(DEN1*PIB1))-2*PIB1*TSB1(M1+1)/DEN1
VRK1B2=-1(((B22-B12)/2.-GAMMA)/(DEN1*PIB2))+2*PIB2*TSB2(M1+1)/DEN1
YB1=VRK1B1/SQRT((B2-B1)/(2*P1))
RO=VRK1B2/VRK1B1
WRITE (IMP,190)VRK1B1,VRK1B2,YB1,RO
190 FORMAT (10X,'K1B1=',F7.4,10X,'K1B2=',F7.4,10X,'YB1=',F7.4,10X,'RO='
5,F7.4)
STOP
3 WRITE (IMP,210)
210 FORMAT (1X,'ARCTANGENTE TE1A3 OU TE1A4 = 0')
STOP
END

```

## ANNEXE A3

DISQUE COMPORTANT TROIS FISSURES SYMÉTRIQUES

MÉTHODE DE SUPERPOSITION

## SUBROUTINE TRUC

```

COMMON TETA(101),RPRO(101),STET(101),A(11,101),CP(11,11),CX(11)
COMMON CY(11),ANUM(11,10),Y(11),Z(11),B(21,21),TSB1(12),TSB2(12)
COMMON RX(10),RY(10),R(21),TSA(12),AP(11,11),SUP(11),X(11)
COMMON /SS/AF,B1,B2,B22,B12,AF2,PI,BETA,M,M1,M3,MM,LC,IMP
DATA A(1,1),A(2,1),A(3,1),A(4,1),A(5,1)/0.,0.,0.,0.,0./
DATA A(6,1),A(7,1),A(8,1),A(9,1),A(10,1)/0.,0.,0.,0.,0./
DATA A(11,1)/0./

```

## C CALCUL NUMERIQUE DES INTEGRALES

```

C *****

```

```

H=PI/(20*M)

```

```

NDIM=11

```

```

L=0

```

```

NM=10*M-9

```

```

DO 300 I=1,NM,10

```

```

L=L+1

```

```

DO 302 N=1,M1

```

```

DO 301 J=1,11

```

```

301 Y(J)=A(N,I+J-1)

```

```

CALL BSF(H,Y,Z,NDIM)

```

```

302 ANUM(N,L)=Z(11)

```

```

300 CONTINUE

```

```

UPS1=B1*1.E-03

```

```

UPS2=B2*1.E-03

```

```

X(1)=B1+UPS1

```

```

H=(B2-B1-UPS1-UPS2)/10

```

```

V=SQRT(B22-B12)

```

```

DO 101 N=1,M1

```

```

DO 102 I=1,11

```

```

IF(1.GT.1)X(I)=X(I-1)+H

```

```

X2=X(I)*X(I)

```

```

FD=SQRT((X2-B12)*(X2-AF2)*(B22-X2))

```

```

102 Y(I)=X(I)**(2*N-1)/FD

```

```

CALL BSF(H,Y,Z,NDIM)

```

```

S1=SQRT(2*UPS1)*(B1**(2*N-1))/(V*SQRT(B1))

```

```

S2=SQRT(2*UPS2)*(B2**(2*N-1))/(V*SQRT(B2))

```

```

SUP(N)=Z(11)+S1+S2

```

```

101 CONTINUE

```

```

RETURN

```

```

END

```

```

(S)

```

SUBROUTINE CHOSE

COMMON TETA(101),RPRO(101),STET(101),A(11,101),CP(11,11),CX(11)  
 COMMON CY(11),ANUM(11,10),Y(11),Z(11),B(21,21),TSB1(12),TSB2(12)  
 COMMON RX(10),RY(10),R(21),TSA(12),AF(11,11),SUP(11),X(11)  
 COMMON /SS/AF,B1,B2,B22,B12,AF2,PI,BETA,M,M1,M3,MM,LC,IMP

C CALCUL DE BETA

C \*\*\*\*\*

AK=SQRT((B22-B12)/(B22-AF2))

CALL CEL1(RES,AK,IER)

F=RES

AZ=1

BZ=1-AK\*AK

CALL CEL2(RES,AK,AZ,BZ,IER)

E=RES

CONS=-1/PI

BETA=CONS\*((AF2-B12-B22)/2.+(B22-AF2)\*E/F)

WRITE(IMP,240)

240 FORMAT(////)

C CALCUL DES RESULTANTES DE L'ETAT B

C \*\*\*\*\*

CON=(AF2+B12+B22)/2.

WRITE(IMP,50)

50 FORMAT(1H,30X,'ARC',20X,'RX',20X,'RY',//)

DO 400 J=1,M

RX(J)=CY(J+1)\*(CONS\*(1-AF(2,J+1)+CON\*AF(1,J+1))+BETA\*AF(1,J+1))-

SCY(J)\*(CONS\*(1-AF(2,J)+CON\*AF(1,J))+BETA\*AF(1,J))

RY(J)=-CONS\*(CX(J+1)-CX(J)-ANUM(2,J)+CON\*ANUM(1,J))-BETA\*ANUM(1,J)

S+CY(J+1)\*(CONS\*(CP(2,J+1)-CON\*CP(1,J+1))-BETA\*CP(1,J+1))-CY(J)\*(1\*

SCONS\*(CP(2,J)-CON\*CP(1,J))-BETA\*CP(1,J))

WRITE(IMP,60)J,RX(J),RY(J)

60 FORMAT(32X,I1,17X,F9.6,13X,F9.6,/) )

400 CONTINUE

RETURN

END

(S)

SUBROUTINE B3

COMMON TETA(101),RPRO(101),STET(101),A(11,101),CP(11,11),CX(11)  
 COMMON CY(11),ANUM(11,10),Y(11),Z(11),B(21,21),TSB1(12),TSE2(12)  
 COMMON RX(10),RY(10),R(21),TSA(12),AP(11,11),SUP(11),X(11)  
 COMMON /S5/AF,B1,B2,B22,B12,AF2,PI,BETA,M,M1,M3,MM,LC,IMP

C  
 C CALCUL DES COEFFICIENTS DE LA MATRICE

C \*\*\*\*\*

C  
 C DEFINITION DE LA MATRICE B

C \*\*\*\*\*

DO 500 I=1,M1

DO 501 J=1,M

B(J,I)=2\*(CY(J+1)\*AP(I,J+1)-CY(J)\*AF(I,J))

501 B(J+M1,I)=-2\*(ANUM(I,J)+CY(J+1)\*CP(I,J+1)-CY(J)\*CP(I,J))

500 B(M1,I)=SUP(I)

DO 502 I=1,M

DO 503 J=1,M

K=2\*I-1

L=2\*I-2

IS=10\*J+1

IT=10\*(J-1)+1

B(J,I+M1)=2\*((SIN(K\*TETA(IS))-SIN(K\*TETA(IT)))/K+CY(J+1)\*COS(L\*  
 STETA(IS))-CY(J)\*COS(L\*TETA(IT)))

503 B(J+M1,I+M1)=-2\*(CY(J+1)\*SIN(L\*TETA(IS))-CY(J)\*SIN(L\*TETA(IT)))

502 B(M1,I+M1)=0.

WRITE(IMP,190)

190 FORMAT(////)

C  
 C RESOLUTION DU SYSTEME

C \*\*\*\*\*

DO 600 I=1,M

R(I)=-RX(I)

R(I+M1)=-RY(I)

600 CONTINUE

R(M1)=0.

EPS=0.0000001

CALL GELG(R,B,M3,1,EPS,IER)

IF(IER.NE.0)GO TO 15

RETURN

15 WRITE(IMP,170)IER

170 FORMAT(1H,'ERREUR DANS LA RESOLUTION DU SYSTEME :IER=',I3)

STOP

END

R(S)



## SUBROUTINE MACHIN

```

COMMON TETA(101),RPRO(101),STET(101),A(11,101),CP(11,11),CX(11)
COMMON CY(11),ANUM(11,10),Y(11),Z(11),B(21,21),TSB1(12),TSB2(12)
COMMON RX(10),RY(10),R(21),TSA(12),AF(11,11),SUP(11),X(11)
COMMON /S5/AF,B1,B2,B22,B12,AF2,PI,BETA,M,M1,M3,MM,LC,IMP
DATA CX(1),CY(1),STET(1)/1.,0.,0./
DATA CP(1,1),CP(2,1),CP(3,1),CP(4,1),CP(5,1)/0.,0.,0.,0.,0./
DATA CP(6,1),CP(7,1),CP(8,1),CP(9,1),CP(10,1)/0.,0.,0.,0.,0./
DATA CP(11,1)/0./

```

C

C CALCUL DE X,Y,C1,C3,C5,C7,C9 POUR LES BORNES DES 10 INTERVALLES

C \*\*\*\*\*

```

I=1
DO 200 N=11,MM,10
I=I+1
CX(I)=COS(TETA(N))
CY(I)=SIN(TETA(N))
DO 900 J=1,M1
AF(J,I)=COS((2*J-1)*TETA(N)-STET(N))/RPRO(N)
CP(J,I)=SIN((2*J-1)*TETA(N)-STET(N))/RPRO(N)
900 CONTINUE
200 CONTINUE
RETURN
END

```

(S)

SUBROUTINE BS

COMMON TETA(101),RPRO(101),STET(101),A(11,101),CP(11,11),CX(11)

COMMON CY(11),ANUM(11,10),Y(11),Z(11),B(21,21),TSB1(12),TSB2(12)

COMMON RX(10),RY(10),R(21),TSA(12),AF(11,11),SUP(11),X(11)

COMMON /S5/AF,B1,B2,B22,B12,AF2,PI,BETA,M,M1,M3,MM,LC,IMP

REAL K1A,K1B1,K1B2

DATA TSA(1),TSB1(1),TSB2(1)/0.,0.,0./

C

CALCUL DES COEFFICIENTS D'INTENSITE DE CONTRAINTES

C

\*\*\*\*\*

M2=M+2

DO 700 I=1,M1

TSA(I+1)=TSA(I)+R(I)\*AF\*\*(2\*I-2)

TSB1(I+1)=TSB1(I)+R(I)\*B1\*\*(2\*I-2)

TSB2(I+1)=TSB2(I)+R(I)\*B2\*\*(2\*I-2)

700 CONTINUE

PIB=PI\*BETA

DEN1=SQRT((B12-AF2)\*(B22-AF2))

K1A=1/DEN1\*((B22+B12-AF2)/2-PIB-2\*PI\*TSA(M2))

DEN2=SQRT((B12-AF2)\*(B22-B12))

DEN3=SQRT((B22-AF2)\*(B22-B12))

VRK1A=SQRT(PI\*AF)\*((B12+B22-AF2)/(2\*PI)-BETA-2\*TSA(M2))/DEN1

VRK1B1=SQRT(PI\*B1)\*((AF2+B22-B12)/(2\*PI)-BETA-2\*TSB1(M2))/DEN2

VRK1B2=SQRT(PI\*B2)\*((B22-AF2-B12)/(2\*PI)+BETA+2\*TSB2(M2))/DEN3

ROAB1=VRK1B1/VRK1A

ROAB2=VRK1B2/VRK1A

RO=VRK1B2/VRK1B1

WRITE(IMP,150)

150 FORMAT(1H,35X,'COEFFICIENTS D'INTENSITE DE CONTRAINTES',//)

WRITE(IMP,160)K1A,VRK1A,VRK1B1,VRK1B2

160 FORMAT(10X,'YA=',F7.4,10X,'K1A=',F7.4,10X,'K1B1=',F7.4,10X,'K1B2='  
S,F7.4,//)

WRITE(IMP,170)ROAB1,ROAB2,RO

170 FORMAT(10X,'K1(B1/A)=',F7.4,10X,'K1(B2/A)=',F7.4,10X,'RO=',F7.4)

RETURN

END

(S)

```

COMMON TETA(101),RPRO(101),STET(101),A(11,101),CP(11,11),CX(11)
COMMON CY(11),ANUM(11,10),Y(11),Z(11),B(21,21),TSB1(12),TSB2(12)
COMMON RX(10),RY(10),R(21),TSA(12),AF(11,11),SUP(11),X(11)
COMMON /S5/AF,B1,B2,B22,B12,AF2,PI,BETA,M,M1,M3,MM,LC,IMP
DATA CX(1),CY(1),STET(1)/1.,0.,0./
DATA TETA(1)/0./
LC=7
IMP=8

```

LECTURE DES DONNEES ET INITIALISATION DES PARAMETRES

\*\*\*\*\*

```

READ(LC,10)B2,B1,AF,M
10 FORMAT(3F4.2,I2)
WRITE(IMP,20)B2,B1,AF,M
20 FORMAT(1H ,30X,'B2=',F4.2,10X,'B1=',F4.2,10X,'A=',F4.2,10X,'M=',12
S,///)
B22=B2*B2
AF2=AF*AF
B12=B1*B1
PI=4.*ATAN(1.)
M1=M+1
M3=2*M+1
R01=1-B2
R02=1-B1
R03=1-AF
R04=1+AF
R05=1+B1
R06=1+B2
RPRO(1)=SQRT(R01*R02*R03*R04*R05*R06)
AF(1,1)=1./RPRO(1)
DO 401 J=2,M1
AP(J,1)=AF(1,1)
401 CONTINUE

```

CALCUL DES PARAMETRES AU NIVEAU DES 100 COUPURES

\*\*\*\*\*

```

MM=10*M+1
DO 100 N=2,MM
TETA(N)=(N-1)*PI/(20*M)
SI=SIN(TETA(N))
CO=COS(TETA(N))
IF(TETA(N).EQ.PI/2)CO=0.0000000
TETA1=ATAN(SI/(CO-B2))
TETA2=ATAN(SI/(CO-B1))
TETA3=ATAN(SI/(CO-AF))
IF(TETA1)2,3,4
2 TETA1=PI+TETA1
4 IF(TETA2)5,3,6
5 TETA2=PI+TETA2
6 IF(TETA3)7,3,8
7 TETA3=PI+TETA3
8 TETA4=ATAN(SI/(CO+AF))
TETA5=ATAN(SI/(CO+B1))
TETA6=ATAN(SI/(CO+B2))

```

```
R01=S1/SIN(TETA1)
R02=S1/SIN(TETA2)
R03=S1/SIN(TETA3)
R04=S1/SIN(TETA4)
R05=S1/SIN(TETA5)
R06=S1/SIN(TETA6)
RPRO(N)=SQRT(R01*R02*R03*R04*R05*R06)
STET(N)=(TETA1+TETA2+TETA3+TETA4+TETA5+TETA6)/2.
DO 800 I=1,M1
A(I,N)=-SIN(2*I*TETA(N)-STET(N))/RPRO(N)
800 CONTINUE
100 CONTINUE
CALL LINK('B7')
CALL LINK('B1')
CALL LINK('B2')
CALL LINK('B3')
CALL LINK('B8')
STOP
3 WRITE(IMP,180)
180 FORMAT(1H,'ARCTANGENTE = 0')
STOP
END
```

R(S)

ANNEXE A 4

DISQUE COMPORTANT UNE FISSURE CENTRALE  
TRANSFORMATION CONFORME

```

IMPLICIT DOUBLE PRECISION (A-H,O-Z)
DIMENSION TETA(42),TETZ(42),ROZ(42),A(42),C(42),D(42)
DIMENSION FAC(42),FAS(42),TTZ(42),CON(82)
DIMENSION P(82,82)
DIMENSION R(82),F(84)
REAL K1,K0
DATA LC,INF/105,108/
DATA TETA(1)/0,DO/
DATA TETZ(1),C(1),D(1)/0,DO,0,DO,0,DO/

```

```

LECTURE ET DETERMINATION DES PARAMETRES

```

```

*****

```

```

10 READ(LC,10)AF,N,L,NB
FORMAT(F5.3,I2,I3,I3)
WRITE(INF,70)AF,L,L,LB
70 FORMAT(20X,'AF=',F5.3,20X,'N=',I2,20X,'L=',I3,20X,'M=',I3,/)
M2=M+2
M1=M+1
M3=-M
M4=2*M+2
AF2=1/F*AF
PI=4.00*DATAN(1,DO)
ROF=DSQRT(1,DO-AF2)
ROZ(1)=(1,DO+ROF)/AF

```

```

PAS=PI*(0,5-(1,./L))/N

```

```

DO=100 I=2,NF2

```

```

IF(I=2)2,2,1

```

```

1 TETA(I)=TETA(I-1)+PAS

```

```

GO TO 3

```

```

2 TETA(I)=PI/L

```

```

3 CO=DCOS(TETA(I))

```

```

SI=DSIN(TETA(I))

```

```

T2=2*TETA(I)

```

```

ROF=(1-2*AF2*DCOS(T2)+AF**4)**0,25

```

```

PHI=LATAN2(DSIN(T2),DCOS(T2)-AF2)/2,

```

```

9 ROZ(I)=DSQRT((CO+ROF*DCOS(PHI))**2+(SI+ROF*DSIN(PHI))**2)/AF

```

```

TETZ(I)=DAPCOS((CO+ROF*DCOS(PHI))/(AF*ROZ(I)))

```

```

TP2=2*TETZ(I)

```

```

CDNU=DSIN(TETZ(I))*ROZ(I)*(ROZ(I)*ROZ(I)-1,)

```

```

CON=ROZ(I)+ROZ(I)-DCOS(TP2)

```

```

DEN=(CON+CON+DSIN(TP2)+DSIN(TP2)

```

```

C(I)=CDNU*CON/DEN

```

```

D(I)=CDNU*DSIN(TP2)/DEN

```

```

100 CONTINUE

```

```

CALCUL DES COEFFICIENTS DE LA MATRICE

```

```

*****

```

```

FORMATION DE LA MATRICE DES COEFFICIENTS (2I+2,2N+2)

```

```

*****

```

```

NEP=2*N+1+NB
DO 200 J=2,NP2
M=0
DO 200 I=NE,NBP
M=M+1
JJ=IABS(I)
PCN(I)=(2.0/PI)**(2*JJ)
IJ=J-1
DO 310 II=JI,J
RCZF=POZ(II)**(2*I)
RCZS=RCZF*RCZ(II)
A(II)=(RCZS-(1.0/RCZS))/PCN(M)
FA=2*(2*I+1)*RCZF
TSZ=2*I*TETZ(II)
TTZ(II)=(2*I+1)*TETZ(II)
FAC(II)=FA*DCOS(TSZ)/PCN(M)
FAS(II)=FA*DSIN(TSZ)/PCN(M)
310 CONTINUE
C R(J-1,M)=1/(J)*DSIN(TTZ(J))-1/(J-1)*DSIN(TTZ(J-1))+1*(FAC(J)*C(J)-
SFAC(J-1)*C(J-1)+FAS(J)*D(J)-FAS(J-1)*D(J-1))
R(J+N,M)=-1*(A(J)+DCOS(TTZ(J))-A(J-1)+DCOS(TTZ(J-1))-1*(FAC(J)*L(J)
SJ)-FAC(J-1)*D(J-1)-FAS(J)*C(J)+FAS(J-1)*C(J-1))
200 CONTINUE

VECTEUR RESULTANTE DES ACTIONS SUR LE CONTOUR
*****
R(1)=-1*DCOS(PI/(2*L))/2.00
R(N+2)=-1*DSIN(PI/(2*1))/2.00
DO 400 J=2,NP1
R(J)=0.00
R(J+N+1)=0.00
400 CONTINUE

RESOLUTION DU SYSTEME
*****
I=NN
J=NN
CALL DARRAY(2,I,J,82,82,B,B)
M=NN
EPS=1.0-16
CALL DGELG(R,B,M,1,EPS,IER)
IF(IER.NE.0)GO TO 15
WRITE(IMP,20)
20 FORMAT(36X,'COEFFICIENTS DES TERMES DE LA SERIE DE PHI',///)
WRITE(IMP,30)(I,R(I),I=1,NN)
30 FORMAT(51X,'ALPHA(',I2,')=' ,E11.4,/)

CALCUL DE K1
*****
P(1)=0.00
DO 500 I=1,NN

```

```
P(I+1)=P(I)+(2*(I+NB)-1)*R(I)/PON(I)
500 CONTINUE
K1=2*DSQRT(PI/AF)*P(2*I+3)
K0=DSQRT(AF/PI)
Y=K1/K0
WRITE(IMP,40)
40 FORMAT(///,20X,'FACTEUR D'INTENSITE DE CONTRAINTES',//)
WRITE(IMP,50)K1
50 FORMAT(51Y,'K1=',E11,4)
WRITE(IMP,90)Y
90 FORMAT(//,52X,'Y=',F8,5)
STOP
15 CONTINUE
WRITE(IMP,60)IER
60 FORMAT(14C,'ERREUR DANS LA RESOLUTION DU SYSTEME ; IEE=',I2)
STOP
END
```



## ANNEXE A5

ANNEAU COMPORTANT DEUX FISSURES SYMÉTRIQUES

TRANSFORMATION CONFORME



CALCUL DES PARAMETRES DE FISSURE (REGION 2)  
\*\*\*\*\*

```

RZ(1)=1.
TZ(1)=0.
T(1)=PI/2.
R(1)=RI
FLW=DLOG(1+FL/RI)
DO 100 I=1,NA
R(I+1)=RI+I*FL/NA
RW=DLOG(R(I+1)/RI)
R1=FLW-RW
R2=FLW+RW
R12=DSQRT(R1*R2)
TZ(I+1)=DATAN(RW/R12)
RZ(I+1)=1.
100 T(I+1)=PI/2.

```

CALCUL DES PARAMETRES DE CONTOUR EXTERIEUR (REGION 2)  
\*\*\*\*\*

```

P1=DLOG(RE/RI)
P2=P1+FLW
P3=P1-FLW
NF=NA+1

```

ARC DE CHARGEMENT  
\*\*\*\*\*

```

T(NA+2)=PI/2.
RW=P1
R1=P3
R2=P2
R12=DSQRT(R1*R2)
RZ(NA+2)=(RW+R12)/FLW
TZ(NA+2)=T(NA+2)
R(NA+2)=RE
PSC=PI/100.
PSC2=PSC*PSC
NA3=NA+3
T(NA3)=T(NA+2)-PSC
RW=DSQRT(PSC2+P1*P1)
TW=DATAN(P1/PSC)
R1=DSQRT(PSC2+P3*P3)
R2=DSQRT(PSC2+P2*P2)
T1=DATAN(P3/PSC)
T2=DATAN(P2/PSC)
R12=DSQRT(R1*R2)
T12=(T1+T2)/2.
RZ(NA3)=DSQRT(RW*RW+R1*R2+2*R12*RW*DCOS(TW-T12))/FLW
T(NA3)=DATAN2(RW*DSIN(TW)+R12*DSIN(T12),RW*DCOS(TW)+R12*DCOS(T12))

```

S)

R(NA3)=RE

```

C
C   RESTE DU CONTOUR EXTERIEUR
C
C   *****

```

DT=(T(NA3)-T23)/NB

DO 150 I=1,NB

T(NA3+I)=T(NA3)-DT\*I

PMT=PSC+DT\*I

PMT2=PMT\*PMT

RW=DSQRT(PMT2+P1\*P1)

R1=DSQRT(PMT2+P3\*P3)

R2=DSQRT(PMT2+P2\*P2)

R12=DSQRT(R1\*R2)

TW=DATAN(P1/PMT)

T1=DATAN(P3/PMT)

T2=DATAN(P2/PMT)

T12=(T1+T2)/2.

RZ(NA3+I)=DSQRT(RW\*RW+R1\*R2+2\*R12\*RW\*DCOS(TW-T12))/FLW

TZ(NA3+I)=DATAN2(RW\*DSIN(TW)+R12\*DSIN(T12),RW\*DCOS(TW)+R12\*DCOS(T12))

S12))

150 R(NA3+I)=RE

```

C
C   CALCUL DES PARAMETRES DE CONTOUR COMMUN
C
C   *****

```

NJ=NA3+NB

PMT23=PI/2.-T23

PC=PMT23\*PMT23

DR=(RE-RI)/ND

DO 200 I=1,ND

P(NJ+I)=RE-I\*DR

P4=DLOG(R(NJ+I)/RI)

P5=P4-FLW

P6=P4+FLW

RW=DSQRT(PC+P4\*P4)

R1=DSQRT(PC+P5\*P5)

R2=DSQRT(PC+P6\*P6)

TW=DATAN(P4/PMT23)

T1=DATAN(P5/PMT23)

T2=DATAN(P6/PMT23)

R12=DSQRT(R1\*R2)

T12=(T1+T2)/2.

RZ(NJ+I)=DSQRT(RW\*RW+R1\*R2+2\*R12\*RW\*DCOS(TW-T12))/FLW

TZ(NJ+I)=DATAN2(RW\*DSIN(TW)+R12\*DSIN(T12),RW\*DCOS(TW)+R12\*DCOS(T12))

S))

200 T(NJ+I)=T23

```

C
C   COEFFICIENTS REGION 2
C
C   *****

```

```

C
WRITE(IMP,120)(RZ(I),I=1,35)
120 FORMAT(10(4X,F7.3))
NA=0
NCT=2*(1+NA+NB+ND)
N2=3+NA+NB+ND
NTS=2*(NA+NB+NC+2*ND+2)+1
JPD=NCT+2*(ND+2)
CTC=FL*(2*RI+FL)/(2*FLW*(RI+FL)*(RI+FL))
NCS=(1+NA+NB+ND)/2
NCI=-NCS
L=0
DO 250 N=NCI,NCS
MA=MA+1
MB=MA+2*NCS
NV=IAES(N)
POD(MA)=1.00
B(1,MA)=(-1)**NV*(CTC*(0.500-2*N)-1)
B(1,MB)=(-1)**NV*(CTC*(0.500+2*N)-1)
IF(N.EQ.NCI)B(1,MB)=0.00
DO 300 I=1,N2
IF(I.EQ.N2)GO TO 301
IF(I.EQ.NF)GO TO 300

```

```

C
C
C
C
C
C
PARAMETRES DE BASE
*****

```

```

DO 350 J=1,2
JJ=I+J-1
RZ1(J)=RZ(JJ)**(2*N-1)
RZ20(J)=RZ1(J)*RZ(JJ)
RZ21(J)=RZ20(J)*RZ(JJ)
RZ22(J)=RZ21(J)*RZ(JJ)
RZ23(J)=RZ22(J)*RZ(JJ)
S0TZ(J)=DSIN((2*N-2)*TZ(JJ))
S1TZ(J)=DSIN((2*N-1)*TZ(JJ))
S20TZ(J)=DSIN(2*N*TZ(JJ))
S21TZ(J)=DSIN((2*N+1)*TZ(JJ))
S2TZ(J)=DSIN(2*TZ(JJ))
S2T(J)=DSIN(2*T(JJ))
C0TZ(J)=DCOS((2*N-2)*TZ(JJ))
C1TZ(J)=DCOS((2*N-1)*TZ(JJ))
C20TZ(J)=DCOS(2*N*TZ(JJ))
C21TZ(J)=DCOS((2*N+1)*TZ(JJ))
C2TZ(J)=DCOS(2*TZ(JJ))
C2T(J)=DCOS(2*T(JJ))

```

```

C
C
C
C
C
C
DENOMINATEURS
*****

```

```

RZ2(J)=RZ(JJ)*RZ(JJ)

```

```

RZS(J)=RZ(JJ)*DSIN(TZ(JJ))
DE1256(J)=(RZ2(J)+2*RZS(J)+1)*POD(MA)
DF34(J)=(RZ2(J)-2*RZS(J)+1)*POD(MA)
DF78(J)=RZ2(J)*RZ2(J)+4*RZ2(J)*RZS(J)+2*RZ2(J)*(2-C2TZ(J))+4*RZS(J)
S)+1
DER(J)=(FLW*FLW/(4*RZ2(J)*RZ2(J))*(RZ2(J)*RZ2(J)+2*RZ2(J)+C2TZ(J)+1
S1))*POD(MA)

```

C EXPRESSIONS DE BASE

C \*\*\*\*\*

```

ACM7(J)=2*N/DE1256(J)*(RZ20(J)*C0TZ(J)+RZ1(J)*S1TZ(J))-1/DE78(J)*
S(RZ22(J)*C0TZ(J)+2*RZ21(J)*S1TZ(J)-RZ20(J)*C2TZ(J))
ASM8(J)=2*N/DE1256(J)*(RZ1(J)*C1TZ(J)-RZ20(J)*S0TZ(J))-1/DE78(J)*
S(-RZ22(J)*S0TZ(J)+2*RZ21(J)*C1TZ(J)+RZ20(J)*S20TZ(J))
BCM7(J)=(2*N+1)/DE1256(J)*(RZ20(J)*C20TZ(J)-RZ21(J)*S1TZ(J))-1/
S(DF78(J)*(RZ21(J)*S21TZ(J)+2*RZ22(J)*C20TZ(J)-RZ23(J)*S1TZ(J))
BSM8(J)=-(2*N+1)/DF1256(J)*(RZ20(J)*S20TZ(J)+RZ21(J)*C1TZ(J))-1/
S(DF78(J)*(RZ21(J)*C21TZ(J)-2*RZ22(J)*S20TZ(J)-RZ23(J)*C1TZ(J))
Z(J)=FLW/(2*RZ2(J))*((PI/R(JJ))**2-1)
OM(J)=Z(J)*(RZ2(J)+C2TZ(J))*S2T(J)
DN(J)=Z(J)*(RZ2(J)+C2TZ(J))+C2T(J)
OD(J)=Z(J)+S2TZ(J)+S2T(J)
DD(J)=7(J)+S2TZ(J)+C2T(J)
YA1(J)=RZ21(J)+C1TZ(J)
YA2(J)=RZ20(J)+S20TZ(J)
YB1(J)=RZ21(J)+C21TZ(J)
YB2(J)=RZ22(J)+S20TZ(J)
XA1(J)=RZ21(J)+S1TZ(J)
YA2(J)=RZ20(J)+C20TZ(J)
XB1(J)=RZ21(J)+S21TZ(J)
XB2(J)=RZ22(J)+C20TZ(J)

```

350 CONTINUE

C RESULTANTES REGION 2

C \*\*\*\*\*

```

L=L+1
IF(I.NE.NA)GO TO 302

```

C RESULTANTES SUR DERNIER SEGMENT DE FISSURE

C \*\*\*\*\*

C VERTICALES

C \*\*\*\*\*

```

B(NF,MA)=-(((YA1(1)+YA2(1))/DE1256(1))-((YA1(1)-YA2(1))/DE34(1)))*
S(ACM7(1)*(OM(1)-OD(1))-ASM8(1)*(OD(1)+DN(1))/DER(1))
B(NF,MB)=-(((YB1(1)-YB2(1))/DE1256(1))-((YB1(1)+YB2(1))/DE34(1)))*
S(BCM7(1)*(OM(1)-DD(1))-BSM8(1)*(OD(1)+DN(1))/DER(1))

```

## HORIZONTALES

\*\*\*\*\*

NF2=NF+1+NA+NB+ND

B(NF2,MA)=(-1)\*NV\*(CTC\*(-4+N\*N+N+C.25)-0.5-2\*N)-

S ((XA1(1)-XA2(1))/DE1256(1))+((XA1(1)+XA2(1))/DE34(1))+

S ACM7(1)+(DN(1)+OD(1))+ASM8(1)+(DD(1)-ON(1))/DER(1)

B(NF2,MB)=(-1)\*NV\*(CTC\*(4+N\*N+3\*N+0.25)-2\*N-0.5)-

S ((XB1(1)+XB2(1))/DE1256(1))-((XB2(1)-XB1(1))/DE34(1))+

S (BCM7(1)+(DN(1)+OD(1))+BSM8(1)+(DD(1)-ON(1))/DER(1)

GO TO 300

## RESULTANTES VERTICALES REGION 2

\*\*\*\*\*

302 IF(I.GT.NF)L=I

B(L,MA)=(((YA1(2)+YA2(2))/DE1256(2))-((YA1(2)-YA2(2))/DE34(2))+

S (ACM7(2)+(DN(2)+OD(2))-ASM8(2)+(OD(2)+DN(2))/DER(2))-

S (((YA1(1)+YA2(1))/DE1256(1))-((YA1(1)-YA2(1))/DE34(1))+

S (ACM7(1)+(DN(1)+OD(1))-ASM8(1)+(OD(1)+DN(1))/DER(1))

B(L,MB)=(((YB1(2)-YB2(2))/DE1256(2))-((YB1(2)+YB2(2))/DE34(2))+

VB(L,MB)

S (BCM7(2)+(DN(2)+OD(2))-BSM8(2)+(OD(2)+DN(2))/DER(2))-

S (((YB1(1)-YB2(1))/DE1256(1))-((YB1(1)+YB2(1))/DE34(1))+

S (BCM7(1)+(DN(1)+OD(1))-BSM8(1)+(OD(1)+DN(1))/DER(1))

## RESULTANTES HORIZONTALES REGION 2

\*\*\*\*\*

IHR=L+1+NA+NB+ND

B(IHR,MA)=(((XA1(2)-XA2(2))/DE1256(2))+((XA1(2)+XA2(2))/DE34(2))+

HA(IHR)

S (ACM7(2)+(DN(2)+OD(2))+ASM8(2)+(DD(2)-ON(2))/DER(2))-

S (((XA1(1)-XA2(1))/DE1256(1))+((XA1(1)+XA2(1))/DE34(1))+

S (ACM7(1)+(DN(1)+OD(1))+ASM8(1)+(DD(1)-ON(1))/DER(1))

B(IHR,MB)=(((XB1(2)+XB2(2))/DE1256(2))-((XB2(2)-XB1(2))/DE34(2))+

HB(IHR)

S (BCM7(2)+(DN(2)+OD(2))+BSM8(2)+(DD(2)-ON(2))/DER(2))-

S (((XB1(1)+XB2(1))/DE1256(1))-((XB2(1)-XB1(1))/DE34(1))+

S (BCM7(1)+(DN(1)+OD(1))+BSM8(1)+(DD(1)-ON(1))/DER(1))

IF(I.LT.NJ)GO TO 300

## CONTOUR COMMUN IJ

\*\*\*\*\*

## DEPLACEMENTS HORIZONTAUX REGION 2

\*\*\*\*\*

J2=1

301 IF(I.EQ.K2)J2=2

IHD=I+NCT-NJ+2

IVD=IHD+ND+1

B(IHD,MA)=(ETA\*(YA1(J2)+YA2(J2))/DE1256(J2))+((YA1(J2)-YA2(J2))/

S DE34(J2))- (ACM7(J2)+(DN(J2)+OD(J2))-ASM8(J2)+(OD(J2)+DN(J2))

```

S      J2))) / DER(J2)
B(IHD,MB)=(ETA*(YB1(J2)-YB2(J2)) / DE1256(J2)) + ((YB1(J2)+YB2(J2)) /
S      DE34(J2)) - (BCM7(J2)*(ON(J2)-DD(J2)) - BSM8(J2)*(OD(J2)+DN(
S      J2))) / DER(J2)

```

```

C      DEPLACEMENTS VERTICAUX REGION 2
C      *****
C

```

```

C      B(IVD,MA)=(ETA*(XA1(J2)-XA2(J2)) / DE1256(J2)) - ((XA1(J2)+XA2(J2)) /
S      DE34(J2)) - (ACM7(J2)*(DN(J2)+CD(J2)) + ASM8(J2)*(DD(J2)-
S      DN(J2))) / DER(J2)
C      B(IVD,MB)=(ETA*(XB1(J2)+XB2(J2)) / DE1256(J2)) + ((X92(J2)-XB1(J2)) /
S      DE34(J2)) - (PCM7(J2)*(DN(J2)+OD(J2)) + BSM8(J2)*(DD(J2)-
S      ON(J2))) / DER(J2)
DO 400 J=JRD,MTS
B(J,MA)=0.00
400 B(J,MB)=0.00
IF(N.NE.NCI) GO TO 300
R(NF,MA)=0.00
B(NF2,MB)=0.00
B(L,MB)=0.00
P(IHR,MB)=0.00
B(IHD,MB)=0.00
B(IVD,MB)=0.00
300 CONTINUE
250 CONTINUE
WRITE(IMP,130)(RZ(I),I=1,35)
130 FORMAT(10(4X,F7.3))

```

```

C      COEFFICIENTS REGION 3
C      *****
C

```

```

C      PARAMETRES DE POSITION
C      *****
C

```

```

C      CONTOUR EXTERIEUR
C      *****
C

```

```

DT3=123/NC
P2=1-RI/RE*RI/RE
T3(1)=0.00
R3(1)=RE
NSJ=1+NA+NB
NC1=NC+1
NF3=NC1+ND
NP1=NF3-1
RP(1)=P1
TP(1)=P1/2.
DO 450 I=2,NC1
T3(I)=(I-1)*DT3
P7(I)=RE

```



```

      RP(I)=DSQRT(T3(I)*T3(I)+P1*P1)
450 TP(I)=DATAN2(P1,-T3(I))

```

```

      CONTOUR COMMUN
      *****

```

```

      DO 500 I=1,ND
      LL=I+NC1
      T3(LL)=T23
      R3(LL)=RE-I*DR
      P9=DLG(R3(LL)/RI)
      RP(LL)=DSQRT(T23+T23+P9*P9)
500 TP(LL)=DATAN2(P9,-T23)
      TP(ND+NC1)=PI

```

```

      COEFFICIENTS REGION 3
      *****

```

```

      DO 550 M=1,NP3
      MG=M+NC1+1
      MD=MG+NP3
      POT(M)=1.D0
      DO 600 I=1,NP1
      DO 650 J=1,2
      JJ=I+J-1
      RP3(J)=RP(JJ)**(2*M-3)/POT(M)
      RP2(J)=RP3(J)*RP(JJ)/POT(M)
      RP1(J)=RP2(J)*RP(JJ)/POT(M)
      S1TP(J)=DSIN((2*M-1)*TP(JJ))
      S2TP(J)=DSIN((2*M-2)*TP(JJ))
      C1TP(J)=DCOS((2*M-1)*TP(JJ))
      C2TP(J)=DCOS((2*M-2)*TP(JJ))
      T23Z(J)=(2*M-3)*TP(JJ)+2*T(JJ)
      T22Z(J)=2*T(JJ)-(2*M-2)*TP(JJ)
      S23(J)=DSIN(T23Z(J))
      C23(J)=DCOS(T23Z(J))
      S22(J)=DSIN(T22Z(J))
      C22(J)=DCOS(T22Z(J))
      P7(J)=1.D0-RI/R3(JJ)*RI/R3(JJ)
650 CONTINUE

```

```

      CONTOUR EXTERIEUR
      *****

```

```

      IF(I.GT.NC)GO TO 601

```

```

      RESULTANTES VERTICALES
      *****

```

```

      IRV=JRD+I-1
      B(IRV,PG)=(2*M-2)*(P7(2)*RP3(2)*S23(2)-P7(1)*RP3(1)*S23(1))

```

B(IRV,MD)=-((2\*RP1(2)\*S1TP(2)+P7(2)\*(2\*M-1)\*RP2(2)\*C22(2))-(2\*RP1  
S (1)\*S1TP(1)+P7(1)\*(2\*M-1)\*RP2(1)\*C22(1)))

RESULTANTES HORIZONTALES

\*\*\*\*\*

IRH=IRV+NC

B(IRH,MG)=-((2\*RP2(2)\*S2TP(2)-P7(2)\*(2\*M-2)\*RP3(2)\*C23(2))-(2\*RP2  
S (1)\*S2TP(1)-P7(1)\*(2\*M-2)\*RP3(1)\*C23(1)))

B(IRH,MD)=(2\*M-1)\*(P7(2)\*RP2(2)\*S22(2)-P7(1)\*RP2(1)\*S22(1))

GO TO 600

CONTOUR COMMUN

\*\*\*\*\*

RESULTANTES VERTICALES

\*\*\*\*\*

601 IRV=NSJ+2-NC1+I

B(IRV,MG)=-((2\*M-2)\*(P7(2)\*RP3(2)+S23(2)-P7(1)\*RP3(1)\*S23(1)))

B(IRV,MD)=((2\*RP1(2)\*S1TP(2)+P7(2)\*(2\*M-1)\*RP2(2)\*C22(2))-(2\*RP1  
S (1)\*S1TP(1)+P7(1)\*(2\*M-1)\*RP2(1)\*C22(1)))

RESULTANTES HORIZONTALES

\*\*\*\*\*R\*\*\*\*\*

IRH=IRV+2\*NCS

B(IRH,MG)=((2\*RP2(2)\*S2TP(2)-P7(2)\*(2\*M-2)\*RP3(2)\*C23(2))-(2\*RP2  
S (1)\*S2TP(1)-P7(1)\*(2\*M-2)\*RP3(1)\*C23(1)))

B(IRH,MD)=-((2\*M-1)\*(P7(2)\*RP2(2)\*S22(2)-P7(1)\*RP2(1)\*S22(1)))

DEPLACEMENTS HORIZONTALAUX

\*\*\*\*\*

J3=1

IDH=NC1+2-NC1+I

B(IDH,MG)=-((RP2(J3)\*C2TP(J3)\*EP1+P7(J3)\*(2\*M-2)\*RP3(J3)\*S23(J3)))

B(IDH,MD)=(RP1(J3)\*S1TP(J3)\*EM1+P7(J3)\*(2\*M-1)\*RP2(J3)\*C22(J3))

IF(I.NE.NP1)GO TO 602

IH1=IDH+1

J3=2

B(IH1,MG)=-((RP2(J3)\*C2TP(J3)\*EP1+P7(J3)\*(2\*M-2)\*RP3(J3)\*S23(J3)))

B(IH1,MD)=(RP1(J3)\*S1TP(J3)\*EM1+P7(J3)\*(2\*M-1)\*RP2(J3)\*C22(J3))

DEPLACEMENTS VERTICAUX

\*\*\*\*\*

602 J3=1

IDV=IDH+ND+1

B(IDV,MG)=-((RP2(J3)\*S2TP(J3)\*EM1-P7(J3)\*(2\*M-2)\*RP3(J3)\*C23(J3)))

B(IDV,MD)=-((RP1(J3)\*C1TP(J3)\*EP1-P7(J3)\*(2\*M-1)\*RP2(J3)\*S22(J3)))

```

IF(I.NE.NP1)GO TO 603
IV1=IH1+ND+1
J3=2
B(IV1,MG)=-((RP2(J3)+S2TP(J3)+EM1-P7(J3)*(2*M-2)*RP3(J3)*C23(J3)/)
B(IV1,MD)=-((RP1(J3)+C1TP(J3)+FP1-P7(J3)*(2*M-1)*RP2(J3)*S22(J3)/)
603 DO 700 II=1,NSJ
III=II+NSJ+ND+1
B(II,MG)=0.00
B(II,MD)=0.00
B(III,MG)=0.00
700 B(III,MD)=0.00
B(NSJ+1,MG)=0.00
B(NSJ+1,MD)=0.00
600 CONTINUE
550 CONTINUE
WRITE(IMP,140)((B(I,J),J=1,NTS),I=1,NTS)
140 FORMAT(///,10(3Y,E10.4))

```

```

C
C
C
C
RESULTANTES EXTERIEURES APPLIQUEES
*****

```

```

DO 750 I=1,NTS
750 REX(I)=0.00
REX(NA+2)=-P/2.00

```

```

C
C
C
C
RESOLUTION DU SYSTEME
*****

```

```

I=NTS
J=NTS
CALL DARRAY(2,I,J,101,101,B,B)
EPS=1.D-30
CALL DGELG(REX,B,NTS,1,EPS,IER)
IF(IER.NE.C)GO TO 1000
WRITE(IMP,40)
40 FORMAT(//,20X,'COEFFICIENTS DE LA SERIE ZETA REGION 2',//)
NC2=NCT/2+1
WRITE(IMP,50)((I,REX(I),I,REX(I+NC2)),I=1,NC2)
50 FORMAT(10X,'ALPHA('',I2,'')='',E11.5,18X,'BETA('',I2,'')='',E11.5,/)
WRITE(IMP,60)
60 FORMAT(//,20X,'COEFFICIENTS DE LA SERIE W REGION 3',//)
NP4=NCT+NP3+1
WRITE(IMP,70)((I,REX(I+NCT),I,REX(I+NP4)),I=1,NP3)
70 FORMAT(10X,'GAMMA('',I2,'')='',E11.5,18X,'DELTA('',I2,'')='',E11.5,/)

```

```

C
C
C
C
FACTEUR D'INTENSITE DE CONTRAINTES
*****

```

```

FAC=2*DSQRT(PI)/DSQRT(FLW*RI*DEXP(FLW))
PH2(1)=0.00
DO 800 I=1,NC2

```

```

J=NCI+I-1
JV=IABS(J-1)
OM1=(-1)**JV
PH2(I+1)=PH2(I)+OM1*(REX(I)*(J-0.25)+0.25*REX(I+NC2-1)+
S      (1-2*(2*J+1))/POD(I)
IF(I.EQ.1)PH2(I+1)=PH2(I)+OM1*REX(I)*(J-0.25)
800 CONTINUE
K1=FAC*PH2(NC2+1)
K0=P*DSQRT(FL/PI)/RE
Y=K1/K0
WRITE(IMP,20)
80 FORMAT(//,20X,'FACTEUR D'INTENSITE DE CONTRAINTES ET FACTEUR DE
S  FORME',//)
WRITE(IMP,90)K1,K0
90 FORMAT(20X,'K1=',F8.5,20X,'Y=',F8.5)
STOP
1000 WRITE(IMP,110)IER
110 FORMAT(///,'PROBLEME DE RESOLUTION : IER=',I3)
STOP
END

```

## ANNEXE A6

### MÉTHODE DES DISCONTINUITÉS DE DÉPLACEMENTS

```

IMPLICIT DOUBLE PRECISION(A-H,O-Z)
COMMON DN(100),DT(100),A(100),X(100),Z(100),DCN(100),DCL(100),
1 PN(100),PT(100),KOD(100),BN(100),BT(100),B(200,200),R(200),
S WF(101)
COMMON/S1/FSB(6),FDB(8)
COMMON/S2/TXZN,TXZT,TXXN,TXXT,TZZN,TZZT,DXN,DXT,DZN,DZT
COMMON/S3/DR,EP0D,NINF
DATA IMP,LC/108,105/

```

```

c
60 READ(LC,3,END=66)NUMBS,NUMBC,NUMBCR,NUMOS,NINF,NSYM
NUMBD=0
FAC=1.D0
IF(NUMBCR.EQ.0)GO TO 56
DO 55 I=1,NUMBCR
READ 6,NUM,RAY,TETAD,TETAF,KODE
TETA=(TETAF-TETAD)/NUM
IF(TETA.LT.0.D0)FAC=-1.D0
SW=RAY*DSQRT(2-2*DCOS(TETA))
DO 55 N=1,NUM
NUMBD=NUMBD+1
TETAM=TETAD+(2*N-1)*TETA/2.D0
TED=(N-1)*TETA
TEF=N*TETA
X(NUMBD)=RAY*DCOS(TETAM)
Z(NUMBD)=RAY*DSIN(TETAM)
A(NUMBD)=SW/2
DCL(NUMBD)=FAC*DCOS(TETAM)
DCN(NUMBD)=FAC*DSIN(TETAM)
BN(NUMBD)=-100*(((DCOS(TED)-DCOS(TEF))*DSIN((TED+TEF)/2.D0))
S/(2.D0*DSIN((TEF-TED)/2.D0)))
BT(NUMBD)=100*(((DCOS(TED)-DCOS(TEF))*DCOS((TED+TEF)/2.D0))
S/(2.D0*DSIN((TEF-TED)/2.D0)))
55 KOD(NUMBD)=KODE
56 IF(NUMBC.LE.0)GO TO 61
PRINT 1,NUMBC
DO 57 I=1,NUMBC
READ 2,NUM,RAY,TETAD,TETAF,KODE,TN,TT
TETA=(TETAF-TETAD)/NUM
IF(TETA.LT.0.D0)FAC=-1.D0
SW=RAY*DSQRT(2-2*DCOS(TETA))
DO 57 N=1,NUM
NUMBD=NUMBD+1
TETAM=TETAD+(2*N-1)*TETA/2
X(NUMBD)=RAY*DCOS(TETAM)
Z(NUMBD)=RAY*DSIN(TETAM)
A(NUMBD)=SW/2
DCL(NUMBD)=FAC*DCOS(TETAM)
DCN(NUMBD)=FAC*DSIN(TETAM)
RN(NUMBD)=TN
BT(NUMBD)=TT
KOD(NUMBD)=KODE

```

```

57 CONTINUE
61 READ 4,PR,EMOD,CDIS
   READ 5,AXX,AZZ,AXZ,BXX,BZZ,BXZ
   PRINT 10,NUMBS
   PRINT 11,NUMOS
   IF (NINF)70,65,70
65 PRINT 13
   GOTO 75
66 STOP
70 PRINT 14
75 GOTO (80,85,90,95),NSYM
80 PRINT 15
   GOTO 110
85 PRINT 16
   GOTO 110
90 PRINT 17,CDIS
   GOTO 100
95 PRINT 18,CDIS
100 IF(NINE) 110,105,110
105 PRINT 19
   STOP
110 CONTINUE
   PRINT 20,PR
   PRINT 21,EMOD
   PRINT 23,AXX,BXX
   PRINT 24,AZZ,BZZ
   PRINT 25,AXZ,BXZ

```

C  
C  
C  
C  
EMPLACEMENT, DIMENSION ET ORIENTATION DES DISCONTINUITES DE DEPLACEMENT  
DU CONTOUR

```

PRINT 39
PRINT 40
DO 115N=1,NUMBS
  READ 41,NUM,XB,ZB,XE,ZE,KODE,TN,TT
  XD=(XE-XB)/NUM
  ZD=(ZE-ZB)/NUM
  SW=DSQRT(XD**2+ZD**2)
  DO 115 NI=1,NUM
    NUMBD=NUMBD+1
    X(NUMBD)=XB+(2*NI-1)*XD/2
    Z(NUMBD)=ZB+(2*NI-1)*ZD/2
    DCL(NUMBD)=ZD/SW
    DCN(NUMBD)=-XD/SW
    A(NUMBD)=SW/2
    BN(NUMBD)=TN
    BT(NUMBD)=TT
    KOD(NUMBD)=KODE
115 CONTINUE
116 PRINT 42,(I,KOD(I),X(I),Z(I),A(I),DCN(I),DCL(I),BN(I),BT(I),I=1,
  SNUMBD)

```

C INCLURE LES COMPOSANTES DE TRACTION AU TRAVERS DES BORNES DE DISCONTINUITÉ  
 C DE DEPLACEMENT ET INITIALISER LES VALEURS DES DISCONTINUITÉS  
 C

```

DO 120 N=1,NUMBD
DT(N)=0
DN(N)=0
PXX=BXX+AXX*Z(N)
PZZ=EZZ+AZZ*Z(N)
PXZ=BXZ+AXZ*Z(N)
DN(N)=DCL(N)**2+PXX+DCN(N)**2+PZZ+2*DCN(N)+DCL(N)*PXZ
120 PT(N)=DCN(N)*DCL(N)*(PXX-PZZ)+(DCN(N)**2-DCL(N)**2)*PXZ
DO 150 I=1,NUMBD
KODE=KOD(I)
GO TO (125,130,135,140),KODE

```

```

125 BN(I)=PN(I)-BN(I)
BT(I)=PT(I)-BT(I)
GO TO 150

```

```

130 BN(I)=-BN(I)
BT(I)=-BT(I)
GO TO 150

```

```

135 BN(I)=PN(I)-BN(I)
BT(I)=-BT(I)
GO TO 150

```

```

140 BN(I)=-BN(I)
BT(I)=PT(I)-BT(I)
150 CONTINUE

```

C CALCUL DES COEFFICIENTS D'INFLUENCE  
 C

```

DO 200 J=1,NUMBD
DCLJ=DCL(J)
DCNJ=DCN(J)
ZJ=Z(J)
AH=A(J)
DO 200 I=1,NUMBD
CALL INITIA
XDIS=X(I)-X(J)
ZI=Z(I)
CALL COEFF(XDIS,ZI,AH,ZJ,DCLJ,DCNJ,1)
GO TO (170,155,160,165),NSYM
155 XDIS=X(I)+X(J)
CALL COEFF(XDIS,ZI,AH,ZJ,-DCLJ,DCNJ,-1)
GOTO 170
160 ZDIS=2*CDIS-ZJ
CALL COEFF(XDIS,ZI,AH,ZDIS,DCLJ,-DCNJ,-1)
GO TO 170
165 ZDIS=2*CDIS-ZJ
CALL COEFF(XDIS,ZI,AH,ZDIS,DCLJ,-DCNJ,-1)
XDIS=X(I)+X(J)
CALL COEFF(XDIS,ZI,AH,ZJ,-DCLJ,DCNJ,-1)

```



```

CALL COEFF (XDIS,ZI,AH,ZDIS,-DCLJ,-DCNJ,1)
170 CONTINUE
KODE=KOD(I)
JN=I+NUMBD
JD=J+NUMBD
GO TO (175,180,185,190),KODE
175 B(I,JD)=DCN(I)*DCI(I)*(TXXN-TZZN)+(DCN(I)**2-DCL(I)**2)*TXZN
      B(I,J)=DCN(I)*DCI(I)*(TXXT-TZZT)+(DCN(I)**2-DCL(I)**2)*TXZT
      B(JN,J)=DCL(I)**2*TXXT+DCN(I)**2*TZZT+2*DCN(I)*DCL(J)*TXZT
      B(JN,JD)=DCL(I)**2*TXXN+DCN(I)**2*TZZN+2*DCN(I)*DCL(I)*TXZN
GO TO 200
180 B(I,JD)=DCN(I)*DXN-DCL(I)*DZN
      B(I,J)=DCN(I)*DXT-DCL(I)*DZT
      B(JN,J)=DCL(I)*DXT+DCN(I)*DZT
      B(JN,JD)=DCL(I)*DXN+DCN(I)*DZN
GO TO 200
185 B(I,JD)=DCN(I)*DXN-DCL(I)*DZN
      B(I,J)=DCN(I)*DXT-DCL(I)*DZT
      B(JN,J)=DCL(I)**2*TXXT+DCN(I)**2*TZZT+2*DCN(I)*DCL(I)*TXZT
      B(JN,JD)=DCL(I)**2*TXXN+DCN(I)**2*TZZN+2*DCN(I)*DCL(I)*TXZN
GO TO 200
190 B(I,JD)=DCN(I)*DCL(I)*(TXXN-TZZN)+(DCN(I)**2-DCL(I)**2)*TXZN
      B(I,J)=DCN(I)*DCI(I)*(TXXT-TZZT)+(DCN(I)**2-DCL(I)**2)*TXZT
      B(JN,J)=DCL(I)*DXT+DCN(I)*DZT
      B(JN,JD)=DCL(I)*DXN+DCN(I)*DZN
200 CONTINUE
M1=2*NUMBD
C
C RESOLUTION DES EQUATIONS
C
EPS=1.D-20
DO 400 I=1,NUMBD
R(I)=-BT(I)
400 R(I+NUMBD)=-BN(I)
CALL DARRAY(2,M1,M1,200,200,B,P)
CALL DFELG(R,P,M1,1,EPS,IER)
IF(IER.NE.C)GO TO 380
DO 401 I=1,NUMBD
DT(I)=R(I)
401 DN(I)=R(I+NUMBD)
C
C INCLURE LES DEPLACEMENTS SUR LES COTES POSITIF ET NEGATIF DES DISCONTINUES
C (ET LES COMPOSANTES DE TRACTION) ET ECRIRE LES RESULTATS
C
PRINT 51
WF(1)=0.D0
DO 600 I=1,NUMBD
ZI=Z(I)
SIGXZ=0.
SIGXX=0.

```

```

SIGZZ=0.
UXPOS=0.
UZPOS=0.
UXNEG=0.
UZNEG=0.
DO 570 J=1,NUMBD
CALL INITIA
DCLJ=DCL(J)
DCNJ=DCN(J)
ZJ=Z(J)
AH=A(J)
XDIS=X(I)-X(J)
CALL COEFF (XDIS,ZI,AH,ZJ,DCLJ,DCNJ,1)
IF (I-J) 480,470,480
470 CON=DCNJ
COL=DCLJ
GO TO 490
480 CON=0.
COL=0.
490 CONTINUE
GO TO (560,500,510,520),NSYM
500 XDIS=X(I)+X(J)
CALL COEFF (XDIS,ZI,AH,ZJ,-DCLJ,DCNJ,-1)
GO TO 560
510 ZDIS=2*CDIS-2J
CALL COEFF (XDIS,ZI,AH,ZDIS,DCLJ,-DCNJ,-1)
GO TO 560
520 ZDIS=2*CDIS-2J
CALL COEFF (XDIS,ZI,AH,ZDIS,DCLJ,-DCNJ,-1)
XDIS=X(I)+X(J)
CALL COEFF (XDIS,ZI,AH,ZJ,-DCLJ,DCNJ,-1)
CALL COEFF (XDIS,ZI,AH,ZDIS,-DCLJ,-DCNJ,1)
560 SIGXX=SIGXX+TXXT*DT(J)+TXXN*DN(J)
SIGZZ=SIGZZ+TZTZ*DT(J)+TZZN*DN(J)
SIGXZ=SIGXZ+TXZT*DT(J)+TXZN*DN(J)
UXPOS=UXPOS+DXT*DT(J)+DXN*DN(J)
UZPOS=UZPOS+DZT*DT(J)+DZN*DN(J)
UXNEG=UXNEG+(DXT-CON)*DT(J)+(DXN-COL)*DN(J)
UZNEG=UZNEG+(DZT-COL)*DT(J)+(DZN-CON)*DN(J)
570 CONTINUE
UNEG=DCL(I)*UXNEG+DCN(I)*UZNEG
UNPOS=DCL(I)*UXPOS+DCN(I)*UZPOS
UTNEG=DCN(I)*UXNEG-DCL(I)*UZNEG
UTPOS=DCN(I)*UXPOS-DCL(I)*UZPOS
WF(I+1)=WF(I)+(A(I)*(UNPOS+BN(Y)+UTPOS*BT(I)))-
SN=PN(I)+DCL(I)**2+SIGXX+DCN(I)**2+SIGZZ+2*DCL(I)*DCN(I)*SIGXZ
ST=PT(I)+DCL(I)*DCN(I)*(SIGXX-SIGZZ)+(DCN(I)**2-DCL(I)**2)*SIGXZ
PRINT 52,I,DN(I),UNPOS,UNEG,DT(I),UTPOS,UTNEG,UXPOS,UZPOS,UXNEG,
SUZNEG,SN,ST
600 CONTINUE
PRINT 58,WF(NUMBD+1)

```

```

C
C INTRODUCTION DES CONTRAINTES OU DES DEPLACEMENTS AUX ENDROITS OU L'UN
C VEUT FAIRE UN CALCUL
C

```

```

700 IF (NUMOS) 900,900,700
PRINT 53

```

```

NUMP=0
DO 850 N=1,NUMOS
READ 43,NUM,XB,ZB,XE,ZE
XD=(XE-XB)/NUM
ZD=(ZE-ZB)/NUM
DO 850 NI=1,NUM
NUMP=NUMP+1
XCL=XB+(2*NI-1)*XD/2
ZCL=ZB+(2*NI-1)*ZD/2
SIGXX=BXX+AXX*ZCL
SIGZZ=BZZ+AZZ*ZCL
SIGXZ=BXZ+AXZ*ZCL
UX=0.
UZ=0.

```

```

C
DO 830 J=1,NUMBD
CALL INITIA
DCLJ=DCL(J)
DCNJ=DCN(J)
ZJ=Z(J)
AH=A(J)

```

```

XDIS=XCL-X(J)
CALL COEFF(XDIS,ZCL,AH,ZJ,DCLJ,DCNJ,1)
GOTO (825,800,810,820),NSYM

```

```

800 XDIS=XCL+X(J)
CALL COEFF(XDIS,ZCL,AH,ZJ,-DCLJ,DCNJ,-1)

```

```

GO TO 825
810 ZDIS=2*CDIS-ZJ
CALL COEFF(XDIS,ZCL,AH,ZDIS,DCLJ,-DCNJ,-1)

```

```

GO TO 825
820 ZDIS=2*CDIS-ZJ
CALL COEFF(XDIS,ZCL,AH,ZDIS,DCLJ,-DCNJ,-1)

```

```

XDIS=XCL+X(J)
CALL COEFF(XDIS,ZCL,AH,ZJ,-DCLJ,DCNJ,-1)
CALL COEFF(XDIS,ZCL,AH,ZDIS,-DCLJ,-DCNJ,1)

```

```

825 SIGXX=SIGXX+TXXT*DT(J)+TXXN*DN(J)
SIGZZ=SIGZZ+TZZT*DT(J)+TZZN*DN(J)
SIGXZ=SIGXZ+TXZT*DT(J)+TXZN*DN(J)
UX=UX+DXT*DT(J)+DXN*DN(J)
UZ=UZ+DZT*DT(J)+DZN*DN(J)

```

```

C
830 CONTINUE
PRINT 54 ,NUMP,XCL,ZCL,SIGXX,SIGZZ,SIGXZ,UX,UZ
850 CONTINUE
C

```

900 CONTINUE  
GO TO 60

1 FORMAT(1X,'NOMBRE DE SEGMENTS DE CONTOUR CALCULES : ',I4, '//')  
 2 FORMAT(I4,F8.4,2F10.7,I4,2F10.3)  
 3 FORMAT(6I4)  
 4 FORMAT(F6.2,E11.4,F8.2)  
 5 FORMAT (6F8.2)  
 6 FORMAT(I4,I8.4,2F10.7,I4)  
 10 FORMAT (/ 'NOMBRE DE SEGMENTS DE DROITES (CONTENANT AU MOINS UNE  
 1 DISCONTINUITÉ) UTILISES POUR DETERMINER LES CONTOURS='I4)  
 11 FORMAT (/ 'NOMBRE DE SEGMENTS DE DROITES UTILISES POUR DETERMINER  
 1 LES AUTRES ENDOITS OU L ON VEUT OBTENIR DES RESULTATS='I4)  
 12 FORMAT (/ 'NOMBRE MAXIMUM D ITERATIONS POUR RESOUDRE LES EQUATIONS  
 1='I4)  
 13 FORMAT (/ 'MILIEU SEMI-INFINI. ')  
 14 FORMAT (/ 'SOLUTION EN MILIEU INFINI. ')  
 15 FORMAT (/ 'AUCUNE CONDITION DE SYMETRIE N EST IMPOSEE. ')  
 16 FORMAT (/ 'X=0.00 EST AXE DE SYMETRIE. ')  
 17 FORMAT (/ 'Z='F8.2' EST AXE DE SYMETRIE. ')  
 18 FORMAT (/ 'Y=0.00 ET Z='F8.2' SONT AXES DE SYMETRIE. ')  
 19 FORMAT (/ 'LA DROITE Z=CONST NE PEUT ETRE UN AXE DE SYMETRIE DAN  
 1S UN MILIEU SEMI-INFINI. ')  
 20 FORMAT (/ 'COEFFICIENT DE POISSON DU MILIEU ='F6.2)  
 21 FORMAT (/ 'MODULE D ELASTICITE DU MILIEU ='E11.4)  
 22 FORMAT (/ 'FACTEUR DE RELAXATION ='F6.2)  
 23 FORMAT (/ 'COMPOSANTE XX DU CHAMP DE CONTRAINTES='F8.2' Z+'F8.2)  
 24 FORMAT (/ 'COMPOSANTE ZZ DU CHAMP DE CONTRAINTES ='F8.2' Z+'F8.2)  
 25 FORMAT (/ 'COMPOSANTE XZ DU CHAMP DE CONTRAINTES ='F8.2' Z+'F8.2)  
 39 FORMAT (/ '///' DANS LA LISTE SUIVANTE, LES DIFFERENTES VALEURS DE  
 1 KODE SONT '//' -TRACTION NORMALE ET TANGENTIELLE SONT INDUJ  
 2 TES (KODE=1) '//' -DEPLACEMENTS NORMAUX ET TANGENTIELS INDU  
 3 JTS (KODE=2) '//' -TRACTION NORMALE ET DEPLACEMENT TANGENTI  
 4 EL INDUITS (KODE=3) '//' -TRACTION TANGENTIELLE ET DEPLACE  
 5 MENT NORMAL INDUITS (KODE=4) '//' LES DEPLACEMENTS INDUITS SONT  
 6 APPLQUES SUR LA FACE POSITIVE D UNE DISCONTINUITÉ')  
 40 FORMAT (/ '///' SEGMENT KODE X-COORD Z-COORD HALF  
 SIDTH DIR COS N DIR COS L N. TRACT. (OU DEPL.) T. TRACT. (OU  
 SDEPL.) '//)  
 41 FORMAT (I4,4F12.4,I4,2F12.4)  
 42 FORMAT (I12,I9,3F12.4,2F12.6,2F22.6)  
 43 FORMAT (I4,4F12.4)  
 49 FORMAT (/ '///' NOMBRE D ITERATIONS='I4/' DIFFERENCE MAXIMALE ENTRE  
 S DEUX ITERATIONS SUCCESSIVES='E10.3/ '///)  
 50 FORMAT (/ '///' LE PROCESSUS D ITERATIONS N ARRIVE PAS A CONVERGER  
 S POUR 'I4' ITERATIONS-DIFFERENCE MAXIMALE ENTRE DEUX ITERATIONS  
 S SUCCESSIVES ='E10.3/ '///)  
 51 FORMAT(/, 'SEG UN(TOTAL) UN(POS) UN(NEG) UT(TOTAL)',4A,  
 1 'UT(POS) UT(NEG) UX(POS) UZ(POS) UX(NEG) UZ(NEG)'5X  
 2 'SIG-N SIG-T',//)  
 52 FORMAT(I3,F14.7,F12.6,F10.4,F14.7,F12.6,F9.4,2F11.6,2F10.5,2F8.1)

```
53 FORMAT (/ POINT X-COORD Z-COORD SIGXX SIGZZ  
S SIGXZ UX UZ //)  
54 FORMAT (I8,5F12.4,2F12.8)  
58 FORMAT(//, ' U = 'E21.15)  
380 WRITE(IMP,381)IER  
381 FORMAT(20X,'PROBLEME D'INVERSION;IER=',I4)  
STOP  
END
```

```
SUBROUTINE INITIA  
IMPLICIT DOUBLE PRECISION(A-H,O-Z)  
COMMON/S2/TXZN, TXZT, TXXN, TXXT, TZZN, TZZT, DXN, DXT, DZN, DZT  
TXZN=0.  
TXZT=0.  
TXXN=0.  
TXXT=0.  
TZZN=0.  
TZZT=0.  
DXN=0.  
DXT=0.  
DZN=0.  
DZT=0.  
RETURN  
END
```

```

SUBROUTINE COEFF (X,Z,A,C,DCL,DCN,MULT)
IMPLICIT DOUBLE PRECISION(A-H,O-Z)
COMMON/S1/FSB(6),FDB(8)
COMMON/S2/TXZN,TXZT,TXXN,TXXT,TZZN,TZZT,DXN,DXT,DZN,DZT
COMMON /S3/PR,EMOD,NINF
CON=EMOD/(16*DATAN(1.0)*(1-PR*PR))
COP=1./(16*DATAN(1.0)*(1-PR))
XI=DCN*X-DCL*(Z-C)
ZETA=DCL*X+DCN*(Z-C)
CALL TERMSB(XI,ZETA,A,DCL,DCN)

```

C

```

SXZSBN=CON*ZETA*(DCL*FSB(6)-DCN*FSB(5))
SYZSBN=CON*(FSB(4)+ZETA*(DCN*FSB(6)+DCL*FSB(5)))
SXXSBN=CON*((DCN**2-DCL**2)*FSB(4)+2*DCN*DCL*FSB(3)+ZETA*
S(DCL*FSB(5)+DCN*FSB(6)))
SXXSBN=CON*(2*DCN**2*FSB(3)-2*DCN*DCL*FSB(4)+ZETA*(DCN*FSB(5)-
SDCL*FSB(6)))
SZZSBN=CON*((DCN**2-DCL**2)*FSB(4)+2*DCN*DCL*FSB(3)-ZETA*(DCL*
SFSB(5)+DCL*FSB(6)))
SZZSBN=-CON*(2*DCN*DCL*FSB(4)+2*DCL**2*FSB(3)+ZETA*(DCL*FSB(5)-
S DCL*FSB(6)))

```

C

```

DXSBN=CON*((DCL**2+(DCL**2-DCN**2)*(1-2*PR))*FSB(1)+DCN*DCL*(3-4*
S PR)*FSB(2)+ZETA*(DCL*FSB(4)-DCN*FSB(3)))
DXSBN=CON*(DCN*DCL*(3-4*PR)*FSB(1)+(DCN**2+(DCN**2-DCL**2)*(1-2*
S PR))*FSB(2)+ZETA*(DCN*FSB(4)+DCL*FSB(3)))
DZSBN=CON*(DCL*DCL*(3-4*PR)*FSB(1)+(DCN**2+(DCN**2-DCL**2)*(1-2*
S PR))*FSB(2)-ZETA*(DCL*FSB(3)+DCN*FSB(4)))
DZSBN=CON*(-(DCL**2+(DCL**2-DCN**2)*(1-2*PR))*FSB(1)-DCN*DCL*(3-4*
S PR)*FSB(2)+ZETA*(DCL*FSB(4)-DCN*FSB(3)))

```

C

```

IF (NINF) 150,100,150
100 YIP=DCN*X+DCL*(Z+C)
ZETAP=-DCL*X+DCN*(Z+C)

```

C

```
CALL TERMDB(XIF,ZETAP,A,DCL,DCN)
```

C

```

SXZDBN=CON*((1-4*DCL**2)*Z+DCL*XI-C)*FDB(5)+DCL*(ZETA+4*DCN*Z)*
S FDB(6)+2*Z*((DCL*XI-C)*FDB(7)+DCL*ZETA*FDB(8))
SXZDBN=-CON*(FDB(4)+DCL*(ZETA+4*DCN*Z)*FDB(5)+((1+4*DCL**2)*Z-
S (DCL*XI-C))*FDB(6)+2*Z*(DCL*ZETA*FDB(7)-(DCL*XI-C)*FDB(3)))
SXXDBN=CON*(-(DCN**2-DCL**2)*FDB(4)+2*DCN*DCL*FDB(3)+DCL*(3*ZETA+
S 4*DCN*Z)*FDB(5)-((1-4*DCL**2)*Z+3*(DCL*XI-C))*FDB(6)+2*Z*
S (DCL*ZETA*FDB(7)-(DCL*XI-C)*FDB(8)))
SXXDBN=-CON*(2*(1+DCL**2)*FDB(3)-2*DCN*DCL*FDB(4)+((1+4*DCL**2)*4-
S 3*(DCL*XI-C))*FDB(5)-DCL*(3*ZETA+4*DCN*Z)*FDB(6)-2*Z*((DCL*
S XI-C)*FDB(7)+DCL*ZETA*FDB(8)))
SZZDBN=CON*(2*DCN*DCL*FDB(3)-(DCN**2-DCL**2)*FDB(4)+DCL*(ZETA-4*4*
S DCN)*FDB(5)+((1-4*DCL**2)*Z-DCL*XI+C)*FDB(6)-2*Z*(DCL*
S ZETA*FDB(7)-(DCL*XI-C)*FDB(8)))
SZZDBN=-CON*(2*DCL**2*FDB(3)-2*DCN*DCL*FDB(4)-((1+4*DCL**2)*Z+DCL*

```

S XI-C)\*FDB(5)-DCL\*(ZETA-4\*DCN\*Z)\*FDB(6)+2\*Z\*((DCL\*XI-C)\*  
S FDB(7)+DCL\*ZETA\*FDB(8)))

C DXDBN=COM\*((DCL\*\*2+1-2\*PR)\*FDB(1)-DCN\*DCL\*FDB(2)+((3-4\*PR)\*(DCL\*  
S XI-C)+(1-2\*DCL\*\*2)\*7)\*FDB(3)+DCL\*((3-4\*PR)\*ZETA+2\*DCN\*Z)\*  
S FDB(4)+2\*Z\*((DCL\*XI-C)\*FDB(5)+DCL\*ZETA\*FDB(6)))

DXDBT=-COM\*(-DCN\*DCL\*FDB(1)+(DCN\*\*2+1-2\*PR)\*FDB(2)+DCL\*((3-4\*PR)\*  
S ZETA+2\*DCN\*Z)\*FDB(3)-((3-4\*PR)\*(DCL\*XI-C)-(1+2\*DCL\*\*2)\*Z)\*  
S FDB(4)+2\*Z\*(DCL\*ZETA\*FDB(5)-(DCL\*XI-C)\*FDB(6)))

DZDBN=COM\*(DCN\*DCL\*FDB(1)+(DCN\*\*2-(1+2\*DCN\*\*2)\*(1-2\*PR))\*FDB(2)+  
S DCL\*((3-4\*PR)\*ZETA-2\*DCN\*Z)\*FDB(3)+((1-2\*DCL\*\*2)\*Z-(3-4\*PR)\*  
S (DCL\*XI-C))\*FDB(4)-2\*Z\*(DCL\*ZETA\*FDB(5)-(DCL\*XI-C)\*FDB(6)))

DZDBT=-COM\*((DCL\*\*2+1-2\*PR)\*FDB(1)-DCN\*DCL\*FDB(2)-((1+2\*DCL\*\*2)\*4+  
S (3-4\*PR)\*(DCL\*XI-C))\*FDB(3)-DCL\*((3-4\*PR)\*ZETA-2\*DCN\*Z)\*  
S FDB(4)+2\*Z\*((DCL\*XI-C)\*FDB(5)+DCL\*ZETA\*FDB(6)))

GO TO 200

150 SXZDBN=0.

SXZDBT=0.

SXXDBN=0.

SXXDBT=0.

SZZDBN=0.

SZZDBT=0.

DXDBN=0.

DXDBT=0.

DZDBN=0.

DZDBT=0.

C 200 TXZN=TXZN+SXZSBN+SXZDBN

TXZT=TXZT+MULT\*(SXZSBT+SXZDBT)

TXXN=TXXN+SXXSBN+SXXDBN

TXXT=TXXT+MULT\*(SXXSBT+SXXDBT)

TZZN=TZZN+SZZSBN+SZZDBN

TZZT=TZZT+MULT\*(SZZSBT+SZZDBT)

DXN=DXN+DXSBN+DXDBN

DXT=DXT+MULT\*(DXSBT+DXDBT)

DZN=DZN+DZSBN+DZDBN

DZT=DZT+MULT\*(DZSBT+DZDBT)

RETURN

END



```
SUBROUTINE TRNFSB(XI,ZETA,A,DCL,DCN)  
IMPLICIT DOUBLE PRECISION(A-H,n-2)  
COMMON /S1/FSB(6),FDB(8)
```

```
IF (ZETA) 20,5,20
```

```
5 ARG=DSORT((XI+A)**2/(XI-A)**2)
```

```
IF (DABS(YI)-A) 10,10,15
```

```
10 FSB(1)=4*DCL*DATAN(1.0)+DCN*DLOG(ARG)
```

```
FSB(2)=4*DCN*DATAN(1.0)-DCL*DLOG(ARG)
```

```
GO TO 30
```

```
15 FSB(1)=DCN*DLOG(ARG)
```

```
FSB(2)=-DCL*DLOG(ARG)
```

```
GO TO 30
```

```
20 FSB(1)=F1(XI,ZETA,A,DCL,DCN)
```

```
FSB(2)=F2(YI,ZETA,A,DCL,DCN)
```

```
30 FSB(3)=F3(YI,ZETA,A,DCL,DCN)
```

```
FSB(4)=F4(XI,ZETA,A,DCL,DCN)
```

```
FSB(5)=F5(YI,ZETA,A,DCL,DCN)
```

```
FSB(6)=F6(XI,ZETA,A,DCL,DCN)
```

```
RETURN
```

```
END
```

```
SUBROUTINE TERPDB(XIP,ZETAP,A,DCL,DCN)  
IMPLICIT DOUBLE PRECISION(A-H,O-Z)  
COMMON/S1/FSE(6),FDE(8)
```

```
C  
IF (ZETAP) 50,40,50  
40 ARG=DSORT((XIP+A)**2/(XIP-A)**2)  
FDE(1)=DCL*DLOG(ARG)  
FDE(2)=DCL*DLOG(ARG)  
GO TO 60  
50 FDE(1)=F1(XIP,ZETAP,A,-DCL,DCN)  
FDE(2)=F2(YIP,ZETAP,A,-DCL,DCN)  
60 FDE(3)=F3(XIP,ZETAP,A,-DCL,DCN)  
FDE(4)=F4(YIP,ZETAP,A,-DCL,DCN)  
FDE(5)=F5(YIP,ZETAP,A,-DCL,DCN)  
FDE(6)=F6(YIP,ZETAP,A,-DCL,DCN)  
FDE(7)=F7(YIP,ZETAP,A,-DCL,DCN)  
FDE(8)=F8(YIP,ZETAP,A,-DCL,DCN)
```

```
C  
RETURN  
END
```



```
FUNCTION F1(X,Z,A,DCL,DCN)
IMPLICIT DOUBLE PRECISION(A-F,O-Z)
F1=DCL*(DATA1((X+A)/Z)-DATA1((X-A)/Z))+DCN*(DLOG((X+A)**2+Z*Z)-
SDLOG((X-A)**2+Z*Z))/2
RETURN
END
```

```
FUNCTION F2(X,Z,A,DCL,DCN)
IMPLICIT DOUBLE PRECISION(A-H,O-Z)
F2=DCN*(DATAN((X+A)/Z)-DATAN((X-A)/Z))-DCL*(DLOG((X+A)**2+Z**2)-
SDLOG((X-A)**2+Z**2))/2
RETURN
END
```

```
FUNCTION F3(X,Z,A,DCL,DCN)
IMPLICIT DOUBLE PRECISION(A-H,O-Z)
F3=((DCN**2-DCL**2)*Z-2*DCN*DCL*(X+A))/((X+A)**2+Z*Z)-
S((DCN**2-DCL**2)*Z-2*DCN*DCL*(X-A))/((X-A)**2+Z*Z)
RETURN
END
```

```
FUNCTION F4(X,Z,A,DCL,DCN)
IMPLICIT DOUBLE PRECISION(A-H,O-Z)
F4=-(2*DCN*DCL*Z+(DCN**2-DCL**2)*(X+A))/((X+A)**2+Z*Z)+
S(2*DCN*DCL*Z+(DCN**2-DCL**2)*(X-A))/((X-A)**2+Z*Z)
RETURN
END
```

```
FUNCTION F5(X,Z,A,DCL,DCN)
IMPLICIT DOUBLE PRECISION(A-H,G-Z)
F5=(DCN*(DCN**2-3*DCL**2)*((X+A)**2-Z**2)+2*DCL*(3*DCN**2-DCL**2)*
S(X+A)*Z)/((X+A)**2+Z**2)**2-
S(DCN*(DCN**2-3*DCL**2)*((X-A)**2-Z**2)+2*DCL*(3*DCN**2-DCL**2)*
S(X-A)*Z)/((X-A)**2+Z**2)**2
RETURN
END
```

```
FUNCTION FC(X,Z,A,DCL,DCN)
  IMPLICIT DOUBLE PRECISION(A-H,O-Z)
  F6=(2*DCN*(DCN**2-3*DCL**2)*(X+A)*Z-DCL*(3*DCN**2-DCL**2)*
  S((X+A)**2-Z**2))/((X+A)**2+Z**2)**2-
  S(2*DCN*(DCN**2-3*DCL**2)*(X-A)*Z-DCL*(3*DCN**2-DCL**2)*
  S((X-A)**2-Z**2))/((X-A)**2+Z**2)**2
  RETURN
END
```



```
FUNCTION F7(X,Z,A,DCL,DCN)
```

```
IMPLICIT DOUBLE PRECISION(A-H,C-Z)
```

```
F7=(8*DCN*DCL*(DCN**2-DCL**2)+(X+A)*((X+A)**2-3*Z*Z)+2*(DCN**4-
```

```
S 6*(DCN*DCL)**2+DCL**4)*Z*(Z**2-3*(X+A)**2))/((X+A)**2+Z*Z)**3-
```

```
S (8*DCN*DCL*(DCN**2-DCL**2)*(X-A)*((X-A)**2-3*Z*Z)+2*(DCN**4-
```

```
S 6*(DCN*DCL)**2+DCL**4)*Z*(Z**2-3*(X-A)**2))/((X-A)**2+Z*Z)**3
```

```
RETURN
```

```
END
```

FUNCTION F8(X,Z,A,DCL,DCN)

IMPLICIT DOUBLE PRECISION(A-H,O-Z)

F8=(2\*(DCN\*\*4-6\*(DCN\*DCL)\*\*2+DCL\*\*4)\*(X+A)\*((X+A)\*\*2-3\*Z\*\*2)-8\*DCN\*

S DCL\*(DCN\*\*2-DCL\*\*2)\*Z\*(Z\*\*2-3\*(X+A)\*\*2))/((X+A)\*\*2+Z\*\*2)\*\*3-

S (2\*(DCN\*\*4-6\*(DCN\*DCL)\*\*2+DCL\*\*4)\*(X-A)\*((X-A)\*\*2-3\*Z\*\*2)-8\*DCN\*

S DCL\*(DCN\*\*2-DCL\*\*2)\*Z\*(Z\*\*2-3\*(X-A)\*\*2))/((X-A)\*\*2+Z\*\*2)\*\*3

RETURN

END

SOUS - PROGRAMMES DE RÉOLUTIONS DES  
SYSTÈMES D'ÉQUATIONS LINÉAIRES

SUBROUTINE DARRAY(MODE,I,J,N,M,S,D)

DOUBLE PRECISION S,D

DIMENSION S(48000),D(68000)

NJ=N-I

IF(MODE-1)100,100,120

100 IJ=I\*J+1

NN=N+J+1

DO 110 K=1,J

NN=NN-NI

DO 110 L=1,I

IJ=IJ-1

NN=NN-1

110 D(NN)=S(IJ)

GO TO 140

120 IJ=C.DD

NN=C.DD

DO 130 K=1,J

DO 125 L=1,I

IJ=IJ+1

NN=NN+1

125 S(IJ)=D(NN)

130 NI=NN+NI

140 RETURN

END

```

SUBROUTINE DGELG(R,A,I,N,EPS,IER)
DOUBLE PRECISION R,A,PIV,TB,TOI,PIVI
DIMENSION A((2000),R(260)
IF(N)23,23,1
1 IER=0
PIV=0.D0
MM=N*M
NN=N*M
DO 3 L=1,I,M
TB=DABS(A(L))
IF(TB-PIV)3,3,2
2 PIV=TB
I=L
3 CONTINUE
TCL=LFS*PIV
LST=1
DO 17 K=1,I
IF(PIV)23,23,4
4 IF(IER)7,5,7
5 IF(PIV-TCL)6,6,7
6 IER=K-1
7 PIVT=1.D0/A(1)
J=(I-1)/I
I=I-J*M-K
J=J+1-K
DO 8 L=K,I,M
LL=L+I
TB=PIVI*R(LL)
R(LL)=R(L)
8 R(L)=TB
IF(K=N)9,12,12
9 LE=DELST+M-K
IF(J)12,12,10
10 II=J*M
DO 11 L=LST,LE
TB=A(L)
LL=L+II
A(L)=A(LL)
11 A(LL)=TB
12 DO 13 L=LST,M,M
LL=L+I
TB=PIVI*A(LL)
A(LL)=A(L)
13 A(L)=TB
A(LST)=J
PIV=0.D0
LST=LST+1
J=0
DO 16 II=LST,LE
PIVI=-A(II)
IST=II+N

```

```
J=J+1
DO 15 L=IST,MM,M
LL=L-J
A(L)=A(L)+PIVI*A(LL)
TB=DABS(A(L))
IF(TB-PIV)15,15,14
14 PIV=TB
I=L
15 CONTINUE
DO 16 L=K,MM,M
LL=L+J
16 R(LL)=R(LL)+PIVI*R(L)
17 LST=LST+M
18 IF(M-1)23,22,19
19 IST=MM+M
LST=L+1
DO 21 I=2,M
II=LST-I
IST=IST-LST
L=IST-M
L=A(L)+.500
DO 21 J=II,MM,M
TE=R(J)
LL=J
DO 20 K=IST,MM,M
LL=LL+1
20 TE=TB-A(K)*R(LL)
K=J+L
R(J)=R(K)
21 R(K)=TE
22 RETLRL
23 IER=-1
RETURN
END
```